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Double-diffusive translation of Earth's inner core

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SUMMARY

The hemispherical asymmetry of the inner core has been interpreted as resulting from a high-viscosity mode of inner core convection, consisting in a translation of the inner core. A thermally driven translation, as originally proposed, is unlikely if the currently favoured high values of the thermal conductivity of iron at core conditions are correct. We consider here the possibility that inner core translation results from an unstable compositional gradient, which would develop either because the light elements present in the core become increasingly incompatible as the inner core grows, or because of a possibly positive feedback of the development of the F-layer on inner core convection. Though the magnitude of the destabilizing effect of the compositional field is predicted to be similar to or smaller than the stabilizing effect of the thermal field, the huge difference between thermal and chemical diffusivities implies that double-diffusive instabilities can still arise even if the net buoyancy increases upward. Using linear stability analysis and numerical simulations, we demonstrate that a translation mode can indeed exist if the compositional field is destabilizing, even if the temperature profile is subadiabatic, and irrespectively of the relative magnitudes of the composition and potential temperature gradients. The existence of this double diffusive mode of translation requires that the following conditions are met: (i) the compositional profile within the inner core is destabilizing, and remains so for a duration longer than the destabilization timescale (on the order of 200 Myr, but strongly dependent on the magnitude of the initial perturbation); and (ii) the inner core viscosity is sufficiently large, the required value being a strongly increasing function of the inner core size (e.g. 10^{17} Pa s when the inner core was 200 km in radius, and $\simeq 3 \times 10^{21}$ Pa s at the current inner core size). If these conditions are met, the predicted inner core translation rate is found to be similar to the inner core growth rate, which is more consistent with inferences from the geomagnetic field morphology and secular variation than the higher translation rate predicted for a thermally driven translation.

Key words: Core; Instability analysis; Numerical modelling.

1 INTRODUCTION

Apart from its North–South anisotropy (Poupinet *et al.* 1983; Morelli *et al.* 1986; Woodhouse *et al.* 1986), the most prominent feature of Earth's inner core is the hemispherical dichotomy observed in its seismological properties: the western hemisphere (west from Greenwich) exhibits stronger anisotropy, lower P -wave velocity, and less attenuation than the eastern hemisphere (Tanaka & Hamaguchi 1997; Niu & Wen 2001; Garcia 2002; Irving *et al.* 2009; Deuss *et al.* 2010; Monnereau *et al.* 2010; Waszek *et al.* 2011; Tanaka 2012; Lythgoe *et al.* 2014). This has been proposed to result from either heterogeneous crystallization due to long-term mantle control (Sumita & Olson 1999; Aubert *et al.* 2008; Gubbins *et al.* 2011) or from a thermal convection mode consisting in a translation of the inner core (Alboussière *et al.* 2010; Monnereau *et al.* 2010), which is the focus of this paper. Inner core translation could plausibly explain the hemispherical structure of the inner core, through textural

change of the iron aggregate during the translation (Bergman *et al.* 2010; Monnereau *et al.* 2010; Cormier *et al.* 2011; Geballe *et al.* 2013; Lasbleis *et al.* 2017; Calvet & Margerin 2018), but could also have profound implications for the dynamics and structure of the outer core. If fast enough, translation can result in significant melting on one of the inner core hemisphere. This may be at the origin (Alboussière *et al.* 2010) of the so-called F-layer, a layer of anomalously low P -wave velocity gradient (Souriau & Poupinet 1991) which has been interpreted as an iron-rich, stably stratified layer (Gubbins *et al.* 2008). Inner core translation, by imposing a highly asymmetric buoyancy flux at the base of the outer core, is also a promising candidate (Aubert 2013; Aubert *et al.* 2013; Davies *et al.* 2013) for explaining the existence of the planetary scale eccentric gyre which has been inferred from quasi-geostrophic core flow inversions (Pais & Jault 2008; Gillet *et al.* 2009).

The translation of the inner core proposed by Monnereau *et al.* (2010) and Alboussière *et al.* (2010) is a high-viscosity mode of

thermal convection. Its existence, therefore, requires the temperature profile in the inner core to be superadiabatic. Thermal convection in the inner core may arise because the temperature at the inner core boundary (ICB) decreases with time as the inner core grows. This builds a temperature profile decreasing from the centre outwards, a situation which could lead to convection if the temperature profile is steeper than the adiabat. The temperature profile within the inner core depends on how efficiently heat is extracted from within the inner core, and on the cooling rate at the ICB. Fast inner core growth and low thermal diffusivity promote a steep, possibly superadiabatic temperature profile; slow inner core growth and high thermal diffusivity results in a flatter, subadiabatic temperature profile.

When the thermally driven convective translation of the inner core was proposed, existing experiments and models favoured a rather low value of the inner core thermal conductivity [$36 \text{ W m}^{-1} \text{ K}^{-1}$ according to Stacey & Davis (2008)] making the existence of thermal convection in the inner core likely. However, the value of the thermal conductivity has since been re-evaluated significantly upward, with all published studies arguing for a thermal conductivity higher than $\sim 100 \text{ W m}^{-1} \text{ K}^{-1}$ in the outer core and possibly larger than $200 \text{ W m}^{-1} \text{ K}^{-1}$ in the inner core (Sha & Cohen 2011; de Koker *et al.* 2012; Pozzo *et al.* 2012; Gomi *et al.* 2013; Pozzo *et al.* 2014; Gomi *et al.* 2016; Ohta *et al.* 2016; Zhang *et al.* 2016), with the exception of Konôpková *et al.* (2016) who estimate the core thermal conductivity at $18\text{--}44 \text{ W m}^{-1} \text{ K}^{-1}$. The high thermal conductivity makes thermally driven convection—and translation—in the inner core unlikely (Deguen *et al.* 2013; Labrosse 2014; Pozzo *et al.* 2014; Lythgoe *et al.* 2015).

Compositional convection might be a viable alternative to thermal convection (Gubbins *et al.* 2013; Labrosse 2014; Pozzo *et al.* 2014; Lythgoe *et al.* 2015): an unstable compositional gradient may arise in the inner core either because the light elements present in the core become increasingly incompatible as the inner core grows (Deguen & Cardin 2011; Gubbins *et al.* 2013), or because of a possibly positive feedback of the development of the F-layer on inner core convection (Deguen *et al.* 2013). Modelling of the thermal and compositional evolution of the inner core indicates that the two contributions are similar in magnitude, though the stabilizing thermal effect is likely larger than the destabilizing compositional effect (Labrosse 2014). It is well known that in this configuration, double-diffusive convection can arise owing to the large contrast between the thermal and compositional diffusivities (Stommel *et al.* 1956; Stern 1960; Huppert & Turner 1981). The possibility of double-diffusive convection of the inner core has been suggested by Pozzo *et al.* (2014).

The goal of this paper is to investigate the conditions of existence of inner core translation in a situation where the temperature field is stabilizing (subadiabatic temperature profile) and the composition field destabilizing. The governing equations are presented in Section 2 and numerical methods are briefly discussed in Section 3. A linear stability analysis of the governing equations (Section 4) demonstrates that an instability of double-diffusive type can develop and initiate a translation motion if the compositional field is destabilizing and the temperature field stabilizing. Expressions for the steady-state translation rate are then obtained in Section 5. The deformation induced by lateral temperature and compositional variations is investigated in Section 6. We then use our results to discuss in Section 7 the feasibility of double-diffusive translation of Earth's inner core. The parameters and variables used in this study are summarized in Table 1, with their definitions or values when applicable.

2 GOVERNING EQUATIONS

In this section, we present the systems of equations used here to model thermochemical convection in the inner core, with melting and freezing at the ICB. We present both a set of equations for a viscous (with newtonian rheology) inner core, and a second set of equations strictly valid in the limit of a rigid inner core (infinite viscosity), which will be used in Sections 4 and 5 to investigate the conditions of existence of a double-diffusive mode of translation and obtain analytical expressions for the steady-state translation rate. The rigid inner core set of equations generalizes the treatment presented in Alboussière *et al.* (2010) to take into account time dependence, a compositional field in addition to the thermal field, and non-negligible diffusion.

2.1 Heat and composition transport

We use a potential temperature formulation where we define the potential temperature as $\Theta = T(r, \theta, \varphi, t) - T_{ad}(r, t)$, where $T_{ad}(r, t)$ is the adiabatic temperature profile anchored at the ICB (Deguen & Cardin 2011). Under the assumption that the dissipation number is small (it is about 7×10^{-2} in the inner core) but allowing for temperature variations of the same order of magnitude as adiabatic variations, this allows to obtain from the entropy balance the following transport equation for Θ :

$$\frac{D\Theta}{Dt} = \kappa_T \nabla^2 \Theta + S_T, \quad \Theta(r_{ic}) = 0, \quad (1)$$

where κ_T is the thermal diffusivity and

$$S_T = -\frac{\partial T_{ad}}{\partial t} + \kappa_T \nabla^2 T_{ad} \quad (2)$$

is a source term comparing the effects of the secular decrease of the temperature at the ICB, which helps maintaining a temperature difference across the inner core, with conduction of heat along the adiabat.

The equation for the transport of composition can be written in a mathematically equivalent way (Deguen *et al.* 2013; Lasbleis *et al.* 2015; Lythgoe *et al.* 2015) by defining a potential composition $\chi = c_s - c_s^{icb}$, where $c_s(r, \theta, \varphi, t)$ is the concentration of a given element in the inner core and c_s^{icb} is its concentration at the ICB on the solid side. We denote by c_l^{icb} the concentration on the liquid side of the ICB, assumed to be a function of time only, and by $k = c_s^{icb}/c_l^{icb}$ the equilibrium partition coefficient of this light element at the ICB conditions. With this formulation, the equation of transport of composition writes

$$\frac{D\chi}{Dt} = \kappa_c \nabla^2 \chi + S_c, \quad \chi(r_{ic}) = 0, \quad (3)$$

where κ_c is the compositional diffusivity and

$$S_c = -\frac{dc_s^{icb}}{dt} = -k \frac{dc_l^{icb}}{dt} - c_l^{icb} \frac{dk}{dt}. \quad (4)$$

In the few calculations taking into account the growth of the inner core (Section 7.4), we use a front fixing method which in effect introduces in eqs (1) and (3) an additional radial advection term equal to $\dot{r}_{ic}(r/r_{ic}) \partial \Theta / \partial r$ and $\dot{r}_{ic}(r/r_{ic}) \partial \chi / \partial r$, respectively, where $r_{ic}(t)$ is the radius of the inner core at time t and $\dot{r}_{ic} = dr_{ic}/dt$ is the inner core growth rate. For simplicity, we will only present in what follows a set of equations assuming a constant inner core radius. All the details related to properly taking into account inner core growth can be found in Deguen & Cardin (2011).

Table 1. Definitions of the main parameters and variables used in this study, with representative values or definition when applicable.

Present-day inner core radius ^a	r_{ic}^p	1221 km			
Density in the inner core ^a	ρ	13 000 kg m ⁻³			
Density jump at the ICB ^a	$\Delta\rho$	600 kg m ⁻³			
Gravitational acceleration ^a	g	4.4 m ² s ⁻¹ at the ICB			
Radial gravity gradient ^a	$g' = dg/dr$	3.6×10^{-6} s ⁻²			
Isentropic bulk modulus ^a	K_S	1400 GPa			
Dynamic viscosity ^b	η	10^{11} to 10^{22} Pa s			
Thermal parameters and variables			Compositional parameters and variables		
Temperature	T		Concentration (solid, liquid)	c_s, c_l	
Adiabatic	T_{ad}		Solid/liquid partition coefficient	$k = c_s^{icb}/c_l^{icb}$	
Potential temperature	$\Theta = T - T_{ad}$		Potential composition	$\chi = c_s - c_s^{icb}$	
Thermal diffusivity ^c	κ_T	$0.5\text{--}2 \times 10^{-5}$ m ² s ⁻¹	Compositional diffusivity ^f	κ_c	10^{-12} m ² s ⁻¹
Thermal expansion coefficient ^d	α_T	10^{-5} K ⁻¹	Compositional expansion coefficient ^f	α_c	1
Thermal source term	S_T	eq. (2)	Compositional source term	S_c	eq. (4)
Grüneisen parameter ^d	γ	1.4			
Clapeyron/adiabatic slopes ratio ^e	dT_s/dT_{ad}	1.65			
Relevant timescales					
Phase change timescale	τ_ϕ	~ 1 ky			
Viscous relaxation timescale	τ_η	$\eta/(\Delta\rho g' r_{ic}^2) \sim 5$ min to 0.1 My			
Thermal diffusion timescale ^g	τ_{κ_T}	$r_{ic}^2/\kappa_T \sim 5$ Gy			
Compositional diffusion timescale ^g	τ_{κ_c}	$r_{ic}^2/\kappa_c \sim 5 \times 10^7$ Gy			
Advection timescale	τ_V	r_{ic}/V			
Non-dimensional parameters					
Phase change number	\mathcal{P}	τ_ϕ/τ_η			
Lewis number	Le	$\kappa_T/\kappa_c = \tau_{\kappa_c}/\tau_{\kappa_T} \sim 10^7$			
Buoyancy ratio	\mathcal{B}	$\alpha_T S_T/(\alpha_c S_c)$			
Thermal Rayleigh number	Ra_Θ	eq. (9)	Compositional Rayleigh number	Ra_χ	eq. (9)
	$\mathcal{R}_\Theta = Ra_\Theta/\mathcal{P}$			$\mathcal{R}_\chi = Ra_\chi/\mathcal{P}$	
Thermal Péclet number	Pe_T	τ_{κ_T}/τ_V	Compositional Péclet number	Pe_c	τ_{κ_c}/τ_V

^a From PREM (Dziewonski & Anderson 1981).

^b Yoshida *et al.* (1996); Buffett (1997); Van Orman (2004); Mound & Buffett (2006); Koot & Dumberry (2011); Reaman *et al.* (2011, 2012).

^c corresponding to a thermal conductivity between 50 and 200 W m⁻¹ K⁻¹ (Sha & Cohen 2011; de Koker *et al.* 2012; Pozzo *et al.* 2012; Gomi *et al.* 2013; Pozzo *et al.* 2014; Gomi *et al.* 2016; Konôpková *et al.* 2016; Ohta *et al.* 2016; Zhang *et al.* 2016).

^d Vocadlo (2015).

^e Deguen & Cardin (2011).

^f Gubbins *et al.* (2013).

^g The free-decay timescale of a spherically symmetric field and of a degree 1 heterogeneity in a sphere are respectively $r_{ic}^2/(\alpha_{01}^2 \kappa)$ and $r_{ic}^2/(\alpha_{11}^2 \kappa)$, where $\alpha_{01} = \pi$ and $\alpha_{11} \simeq 4.4934$ are the first zeros of the degree 0 and degree 1 spherical Bessel function of the first kind. This is respectively a factor 9.87 and 20.2 smaller than the timescales given in the table.

2.2 Dimensionless equations

We denote by $\Delta\Theta$ the difference of potential temperature across the inner core, and by $\Delta\chi$ the difference of potential composition across the inner core. The acceleration of gravity is taken to vary linearly with radius, $g(r) = g' r$. Scaling lengths by r_{ic} , time by r_{ic}^2/κ_T , velocity by κ_T/r_{ic} , temperature by $\Delta\Theta$, and composition by $\Delta\chi$, the equations of conservation of momentum, continuity, heat and composition transport write

$$0 = -\nabla p + \left(Ra_\Theta \Theta + \frac{Ra_\chi}{Le} \chi \right) \mathbf{r} + \nabla^2 \mathbf{u}, \quad (5)$$

$$\nabla \cdot \mathbf{u} = 0, \quad (6)$$

$$\frac{D\Theta}{Dt} = \nabla^2 \Theta + \frac{S_T r_{ic}^2}{\kappa_T \Delta\Theta}, \quad (7)$$

$$Le \frac{D\chi}{Dt} = \nabla^2 \chi + \frac{S_c r_{ic}^2}{\kappa_c \Delta\chi}, \quad (8)$$

where p is the dynamic pressure, \mathbf{u} the velocity, $\mathbf{r} = r \mathbf{e}_r$. The thermal and compositional Rayleigh numbers and the Lewis number are defined as

$$Ra_\Theta = \frac{\alpha_T \rho g' \Delta\Theta r_{ic}^4}{\kappa_T \eta}, \quad Ra_\chi = \frac{\alpha_c \rho g' \Delta\chi r_{ic}^4}{\kappa_c \eta}, \quad Le = \frac{\kappa_T}{\kappa_c}, \quad (9)$$

where α_T and α_c are the thermal and compositional expansion coefficients, ρ the density of the inner core and η the dynamic viscosity.

Following Alboussière *et al.* (2010), we assume that melting and freezing happens at the ICB at a rate proportional to the topography h of the ICB, and inversely proportional to a timescale τ_ϕ which depends on how efficiently convection in the outer core is able to transport the latent heat associated with melting or freezing. If the topography varies slowly with time compared to τ_ϕ [estimated to be ~ 1 kyr (Alboussière *et al.* 2010)], this amounts to state that the

radial velocity u_r at the ICB is

$$u_r = \frac{h}{\tau_\phi}. \quad (10)$$

Using this phase change law to relate the radial velocity at the ICB to the topography, the continuity of normal stress across the ICB can be written as

$$-2\eta \frac{\partial u_r}{\partial r} + p = \Delta\rho g(r_{ic}) \tau_\phi u_r \quad (11)$$

(Deguen *et al.* 2013), where $\Delta\rho$ is the density jump across the ICB. Once made dimensionless, this can be written as

$$-2 \frac{\partial u_r}{\partial r} + p = \mathcal{P} u_r, \quad (12)$$

where

$$\mathcal{P} = \frac{\Delta\rho g' r_{ic}^2 \tau_\phi}{\eta} \quad (13)$$

is the ‘phase change number’ introduced in Deguen *et al.* (2013), which quantifies the resistance to phase change at the ICB. \mathcal{P} is the ratio of τ_ϕ to the timescale $\eta/(\Delta\rho g(r_{ic}) r_{ic})$, which is best understood in this context as the time needed to build from zero a topography balancing the internal stresses: Consider a flow within the inner core with a radial velocity u_r varying radially over the lengthscale r_{ic} . Starting from a state with no topography, this flow will deform the ICB up to a point where the normal stress at $r = r_{ic}$, which is $\sim \eta u_r / r_{ic}$, is balanced by the topography weight $\sim \Delta\rho g(r_{ic}) h$. This happens when $h \sim \eta u_r / (\Delta\rho g(r_{ic}) r_{ic})$. The time needed to build this topography is $h/u_r \sim \eta/(\Delta\rho g(r_{ic}) r_{ic})$.

In the limit of infinite \mathcal{P} , the boundary condition (12) reduces to the condition $u_r = 0$, which corresponds to impermeable conditions. In this limit, the timescale of topography building is short compared to the phase change timescale, which implies the formation of a topography balancing the internal stresses.

In contrast, when $\mathcal{P} \rightarrow 0$, eq. (12) implies that the normal stress tends towards 0 at the ICB, which corresponds to fully permeable boundary conditions. In this limit, the timescale of topography building is long compared to the phase change timescale, which implies that phase change is too fast to allow the development of a topography balancing the internal stresses.

The general case of finite \mathcal{P} gives boundary conditions for which the rate of phase change at the boundary (equal to u_r) is proportional to the normal stress induced by convection within the inner core.

We further impose shear stress free conditions. By construction, $\Theta = \chi = 0$ at the ICB.

2.3 The rigid inner core limit

In the limit of a rigid inner core (no deformation allowed), the possible motions of the inner core are restricted to either rotational motions (which we will not consider here) and translation motions, which can arise in response to degree 1 density heterogeneities in the inner core.

An expression for the translation rate can be obtained by combining the phase change law eq. (10) with the force balance on the inner core, which we use to obtain the displacement of the inner core from a reference state as a function of the internal density distribution. The force balance on the inner core comes down to an equilibrium between buoyancy forces associated with density anomalies within the inner core and pressure forces applied by the outer core on the inner core surface. This force balance gives the displacement of the inner core and the degree 1 component h_1 of the ICB topography.

Using the phase change law eq. (10) to relate the translation rate V to h_1 through $V = h_1/\tau_\phi$, we obtain the following expression for the translation rate:

$$V = \frac{\rho}{\Delta\rho r_{ic}^3 \tau_\phi} \int_0^{r_{icb}} [\alpha_T \Theta_1(r) + \alpha_c \chi_1(r)] r^3 dr \quad (14)$$

(see Appendix A1 for the derivation). Once made dimensionless, this writes

$$V = \int_0^1 \left(\mathcal{R}_\Theta \Theta_1 + \frac{\mathcal{R}_\chi}{Le} \chi_1 \right) r^3 dr, \quad (15)$$

where

$$\mathcal{R}_\Theta = \frac{\alpha_T \rho \Delta \Theta r_{ic}^2 / \kappa_T}{\Delta\rho \tau_\phi} = \frac{Ra_\Theta}{\mathcal{P}}, \quad (16)$$

$$\mathcal{R}_\chi = \frac{\alpha_c \rho \Delta \chi r_{ic}^2 / \kappa_c}{\Delta\rho \tau_\phi} = \frac{Ra_\chi}{\mathcal{P}}.$$

\mathcal{R}_Θ and \mathcal{R}_χ are independent of the viscosity, as appropriately defined non-dimensional numbers should be since here no deformation is allowed. Note that they are also independent of the acceleration of gravity.

In the translation mode, the potential temperature and composition fields are symmetric about the translation direction, and the equations of transport of heat and composition are given by eqs (1) and (3) in which advective transport is restricted to the translation direction:

$$\frac{\partial \Theta}{\partial t} + \mathbf{V} \cdot \nabla \Theta = \nabla^2 \Theta + \frac{S_T r_{ic}^2}{\kappa_T \Delta \Theta}, \quad \Theta(r_{ic}) = 0, \quad (17)$$

$$Le \left(\frac{\partial \chi}{\partial t} + \mathbf{V} \cdot \nabla \chi \right) = \nabla^2 \chi + \frac{S_c r_{ic}^2}{\kappa_c \Delta \chi}, \quad \chi(r_{ic}) = 0, \quad (18)$$

where \mathbf{V} is the translation velocity. Expanding Θ and χ as series of Legendre polynomials of $\cos \theta$, where θ is the angle between \mathbf{r} and the translation direction, eqs (17) and (18) can then be written, as demonstrated in Appendix A2, as

$$\begin{aligned} \frac{\partial \Theta_l}{\partial t} = & -V \frac{l+1}{2l+3} \left(\frac{l+2}{r} + \frac{\partial}{\partial r} \right) \Theta_{l+1} \\ & + V \frac{l}{2l-1} \left(\frac{l-1}{r} - \frac{\partial}{\partial r} \right) \Theta_{l-1} \\ & + \mathcal{D}_l \Theta_l + \frac{S_T r_{ic}^2}{\kappa_T \Delta \Theta} \delta_{0l}, \quad \forall l \geq 0, \end{aligned} \quad (19)$$

$$\begin{aligned} \frac{\partial \chi_l}{\partial t} = & -V \frac{l+1}{2l+3} \left(\frac{l+2}{r} + \frac{\partial}{\partial r} \right) \chi_{l+1} \\ & + V \frac{l}{2l-1} \left(\frac{l-1}{r} - \frac{\partial}{\partial r} \right) \chi_{l-1} \\ & + \frac{1}{Le} \left(\mathcal{D}_l \chi_l + \frac{S_c r_{ic}^2}{\kappa_c \Delta \chi} \delta_{0l} \right), \quad \forall l \geq 0, \end{aligned} \quad (20)$$

which have to be solved together with the boundary conditions $\Theta_l(r=1) = \chi_l(r=1) = 0$. The operator \mathcal{D}_l is defined as

$$\mathcal{D}_l = \frac{d^2}{dr^2} + \frac{2}{r} \frac{d}{dr} - \frac{l(l+1)}{r^2}. \quad (21)$$

3 NUMERICAL METHODS

In the following sections, we will perform a linear stability analysis of double-diffusive convection with a phase-change interface

(Section 4), derive analytical solutions for the steady-state translation rate (Section 5) and quantify the conditions of existence of the translation mode (Section 6). The theoretical predictions will be compared with numerical simulations obtained by running two different codes: the first one [an extension of the code used in Deguen *et al.* (2013)] solves the Stokes equation and the temperature and composition transport equations, and has been used here in an axisymmetric configuration; the second is a simpler code only allowing the translation mode, the evolution of which is obtained by solving eqs (15), (19) and (20). The latter approach has the advantage of being highly efficient (the Stokes equation does not need to be solved, and the nonlinear term of the advection equations is solved in the spectral domain).

Up to 512 radial levels and maximal harmonic degree of 256 have been used. Care has been taken to always correctly resolve the compositional boundary layer below the ICB, which can be quite thin.

4 ONSET OF DOUBLE-DIFFUSIVE CONVECTION

4.1 Marginal stability

We consider here an initial state at rest, with the potential temperature and composition fields following spherically symmetric profiles $\bar{\Theta}(r)$ and $\bar{\chi}(r)$. This state is perturbed by infinitesimal perturbations $\Theta'(r, \theta, \phi, t)$ and $\chi'(r, \theta, \phi, t)$, and we write

$$\Theta(r, \theta, \phi, t) = \bar{\Theta}(r) + \Theta'(r, \theta, \phi, t), \quad (22)$$

$$\chi(r, \theta, \phi, t) = \bar{\chi}(r) + \chi'(r, \theta, \phi, t). \quad (23)$$

The evolution of the perturbations is controlled by the equations of conservation of momentum, heat and composition given by eqs (5), (1) and (3).

Taking twice the curl of the Stokes, eq. (5) gives

$$0 = -\nabla^2 \left(Ra_\Theta \Theta' + \frac{Ra_\chi}{Le} \chi' \right) \mathbf{r} - \nabla^4 \mathbf{u}, \quad (24)$$

where $\nabla^4(\dots) = \nabla \times \nabla \times \nabla \times \nabla \times (\dots)$. Linearizing the heat and composition transport equations gives

$$u_r \frac{\partial \bar{\Theta}}{\partial r} = \nabla^2 \Theta', \quad (25)$$

$$u_r \frac{\partial \bar{\chi}}{\partial r} = \frac{1}{Le} \nabla^2 \chi'. \quad (26)$$

Multiplying eq. (25) by Ra_Θ , eq. (26) by Ra_χ and adding the two equations, gives

$$u_r \left(Ra_\Theta \frac{\partial \bar{\Theta}}{\partial r} + Ra_\chi \frac{\partial \bar{\chi}}{\partial r} \right) = \nabla^2 \left(Ra_\Theta \Theta' + \frac{Ra_\chi}{Le} \chi' \right), \quad (27)$$

which we inject into eq. (24) to obtain

$$0 = u_r \left(Ra_\Theta \frac{\partial \bar{\Theta}}{\partial r} + Ra_\chi \frac{\partial \bar{\chi}}{\partial r} \right) \mathbf{r} + \nabla^4 \mathbf{u}. \quad (28)$$

This can be solved with the boundary conditions given by the continuity of stress at the ICB (eq. 12 plus shear-stress-free conditions).

Assuming for illustration that the base profiles $\bar{\Theta}$ and $\bar{\chi}$ have the same r dependency, this gives the exact same equation as would have been obtained in the case of purely thermal convection, with

$Ra_\Theta + Ra_\chi$ instead of Ra_Θ . In this case, the results on the marginal stability of thermal convection in the inner core obtained in Deguen *et al.* (2013) can be extended to the case of two-components convection by simply replacing Ra_Θ by $Ra_\Theta + Ra_\chi$. Instability requires that

$$Ra_\Theta + Ra_\chi > Ra_{cr}(\mathcal{P}), \quad (29)$$

where the critical Rayleigh number Ra_{cr} is a function of \mathcal{P} , which can be calculated numerically as explained in Deguen *et al.* (2013). Ra_{cr} is well approximated by

$$Ra_{cr} = \begin{cases} \frac{175}{2} \mathcal{P} & \text{if } \mathcal{P} \ll 10^2, \\ 1545.6 & \text{if } \mathcal{P} \gg 10^2. \end{cases} \quad (30)$$

Eq. (29) demonstrates that the convection instability can develop even when the sum of the thermal and compositional buoyancy $\alpha_T \Theta + \alpha_c \chi$ increases upward: since $\kappa_c \ll \kappa_T$, $Ra_\Theta + Ra_\chi$ can be positive with $Ra_\Theta < 0$ ($\Delta\Theta < 0$) even if $|\alpha_T \Delta\Theta| > |\alpha_c \Delta\chi|$. This is typical of double-diffusive convection, and a direct consequence of the differential diffusion of the thermal and compositional fields: convective motions can develop because the much larger thermal diffusivity allows temperature heterogeneities to diffuse much faster than compositional heterogeneities.

The mathematical analogy at the marginal state between the two-components case and the thermal case also holds when calculating the first unstable mode. The analysis of Deguen *et al.* (2013; Section 4), thus, implies that the first unstable mode consists in a translation if $\mathcal{P} \lesssim 30$. In this limit, taking $Ra_{cr} = \frac{175}{2} \mathcal{P}$ and dividing eq. (29) by \mathcal{P} gives the following criterion for instability:

$$\mathcal{R}_\Theta + \mathcal{R}_\chi > \frac{175}{2}. \quad (31)$$

Again, the instability criterion can be met even when $\alpha_T \Theta + \alpha_c \chi$ increases upwards if $\kappa_c \ll \kappa_T$, suggesting that a double-diffusive translation mode is possible.

4.2 The $\mathcal{P} \rightarrow 0$ limit

4.2.1 Marginal stability

If we restrict ourselves to the emergence of the translation mode, the critical value of \mathcal{R}_Θ and \mathcal{R}_χ for more general forms of the potential temperature and composition profiles can be found by analysing the set of equations developed in Section 2.3 for a pure translation. The inner core is unstable against the translation instability if any arbitrarily small perturbations of the degree one components of the thermal and compositional fields initially grow with time, that is, if

$$\frac{1}{\Theta_1} \frac{\partial \Theta_1}{\partial t} = \frac{1}{\Theta_1} \left[-V \frac{2}{5} \left(\frac{3}{r} + \frac{\partial}{\partial r} \right) \Theta_2 - V \frac{\partial \Theta_0}{\partial r} + \mathcal{D}_1 \Theta_1 \right] > 0, \quad (32)$$

$$\frac{1}{\chi_1} \frac{\partial \chi_1}{\partial t} = \frac{1}{\chi_1} \left[-V \frac{2}{5} \left(\frac{3}{r} + \frac{\partial}{\partial r} \right) \chi_2 - V \frac{\partial \chi_0}{\partial r} + \frac{\mathcal{D}_1 \chi_1}{Le} \right] > 0. \quad (33)$$

The marginal stability state (neither growth or decay of any infinitesimal perturbations) corresponds to $\partial \Theta_1 / \partial t = \partial \chi_1 / \partial t = 0$. Linearizing eqs (32) and (33) and keeping only terms of order 1 in perturbation quantities (i.e. ignoring the terms in $V\Theta_2$ and $V\chi_2$), the marginal stability state corresponds to

$$0 = -V \frac{\partial \Theta_0}{\partial r} + \mathcal{D}_1 \Theta_1, \quad (34)$$

$$0 = -V \frac{\partial \chi_0}{\partial r} + \frac{1}{Le} \mathcal{D}_1 \chi_1. \quad (35)$$

At this stage, we let the mathematical forms of Θ_0 and χ_0 unspecified and just write

$$\Theta_1 = V \mathcal{D}_1^{-1} \left\{ \frac{\partial \Theta_0}{\partial r} \right\} \quad \text{and} \quad \chi_1 = Le V \mathcal{D}_1^{-1} \left\{ \frac{\partial \chi_0}{\partial r} \right\} \quad (36)$$

the solutions of eqs (34) and (35) which vanish at $r = 1$, as must Θ_1 and χ_1 . Injecting these expressions in eq. (15) gives the following relation between \mathcal{R}_Θ and \mathcal{R}_χ at marginal stability:

$$\mathcal{R}_\Theta \int_0^1 \mathcal{D}_1^{-1} \left\{ \frac{\partial \Theta_0}{\partial r} \right\} r^3 dr + \mathcal{R}_\chi \int_0^1 \mathcal{D}_1^{-1} \left\{ \frac{\partial \chi_0}{\partial r} \right\} r^3 dr = 1. \quad (37)$$

The critical values of \mathcal{R}_Θ and \mathcal{R}_χ corresponding to either purely thermal or purely compositional convection are given by

$$\mathcal{R}_{\Theta,cr} = \left[\int_0^1 \mathcal{D}_1^{-1} \left\{ \frac{\partial \Theta_0}{\partial r} \right\} r^3 dr \right]^{-1}, \quad (38)$$

$$\mathcal{R}_{\chi,cr} = \left[\int_0^1 \mathcal{D}_1^{-1} \left\{ \frac{\partial \chi_0}{\partial r} \right\} r^3 dr \right]^{-1}, \quad (39)$$

which will be calculated explicitly below for given forms of the temperature and compositional profiles. Convection sets in if

$$\frac{\mathcal{R}_\Theta}{\mathcal{R}_{\Theta,cr}} + \frac{\mathcal{R}_\chi}{\mathcal{R}_{\chi,cr}} > 1. \quad (40)$$

Let us now evaluate $\mathcal{R}_{\Theta,cr}$ and $\mathcal{R}_{\chi,cr}$ for different forms of the thermal or compositional profiles. Taking into account the variation of the partition coefficient with temperature (Gubbins *et al.* 2013), Labrosse (2014) found that the composition profile in the inner core is well approximated by

$$\chi_0 = \frac{\frac{3}{2} r_{ic}^* (1 - r^2) - (1 - r^3)}{\frac{3}{2} r_{ic}^* - 1}, \quad (41)$$

where r_{ic}^* is the inner core radius (here normalized by the current inner core radius) at which the effect of the secular enrichment of the outer core in incompatible elements becomes dominant over the effect of the variation of the partition coefficient with temperature. The radial composition gradient is then given by

$$\frac{\partial \chi_0}{\partial r} = -2 \frac{r^2 - r_{ic}^* r}{2/3 - r_{ic}^*}. \quad (42)$$

The critical value of \mathcal{R}_χ is thus given by

$$\mathcal{R}_{\chi,cr} = \frac{r_{ic}^* - 2/3}{2} \left[\int_0^1 \mathcal{D}_1^{-1} \{ r^2 - r_{ic}^* r \} r^3 dr \right]^{-1}. \quad (43)$$

It can be verified that, for any number α , the solution of the equation $\mathcal{D}_1(x) = r^\alpha$ which vanishes at $r = 1$ is

$$\mathcal{D}_1^{-1}(r^\alpha) = \frac{r^{\alpha+2} - r}{\alpha^2 + 5\alpha + 4}. \quad (44)$$

Using this expression, we find from eq. (43) that

$$\mathcal{R}_{\chi,cr} = 80 \frac{\frac{3}{2} r_{ic}^* - 1}{\frac{48}{35} r_{ic}^* - 1}. \quad (45)$$

The case of a constant partition coefficient k corresponds to the limit $r_{ic}^* = 0$ in eq. (45), which gives

$$\mathcal{R}_{\chi,cr} = 80. \quad (46)$$

In the thermal case, the basic potential temperature profile is set by an equilibrium between cooling and thermal diffusion (Deguen & Cardin 2011). The potential temperature difference across the inner core is given by $\Delta\Theta = S_T r_{ic}^2 / (6\kappa_T)$, and the non-dimensional temperature profile is given by $1 - r^2$, which corresponds mathematically to the limit $r_{ic}^* \rightarrow \infty$ in eq. (45). This gives

$$\mathcal{R}_{\Theta,cr} = \frac{175}{2} = 87.5, \quad (47)$$

in agreement with the value found by Deguen *et al.* (2013) from a more general linear stability analysis (not restricted to the translation mode).

In the case of a positive \mathcal{R}_χ and negative \mathcal{R}_Θ , the instability condition eq. (40) can be recast as

$$\frac{\alpha_c \Delta\chi}{-\alpha_T \Delta\Theta} > \left(\frac{\mathcal{R}_{\chi,cr}}{\mathcal{R}_{\Theta,cr}} - \frac{\mathcal{R}_{\chi,cr}}{\mathcal{R}_\Theta} \right) Le^{-1}. \quad (48)$$

\mathcal{R}_Θ and \mathcal{R}_χ are both expected to be large in magnitude compared with their critical values. Since in addition the critical values $\mathcal{R}_{\Theta,cr}$ and $\mathcal{R}_{\chi,cr}$ are of the same order of magnitude, the condition for instability in practice reduces to

$$\frac{-\alpha_T \Delta\Theta}{\alpha_c \Delta\chi} \lesssim Le. \quad (49)$$

$Le \simeq 2 \times 10^7$ in the inner core (Gubbins *et al.* 2013), which implies that the inner core can be unstable against the translation instability even if the magnitude of the destabilizing compositional density gradient is much smaller than a stabilizing thermal density gradient. Labrosse (2014) obtained values of $\frac{\alpha_T \Delta\Theta}{\alpha_c \Delta\chi}$ ranging from about -5 to positive values, depending on the outer core composition and assumptions on the evolution of the core. In what follows, we will take -3 as a representative value of the stabilizing thermal stratification/destabilizing compositional stratification case.

4.2.2 Growth rate of the translation instability

Though instability appears almost unavoidable when the compositional profile is destabilizing, whether the translation rate eventually becomes significant depends on the growth rate σ of the instability compared to the inner core age, and on the magnitude of the initial perturbations. It is, therefore, useful to estimate the growth rate of the instability when the conditions are supercritical. This is done in Appendix A3, where the growth rate is obtained by decomposing the spherical harmonics degree 1 component of the composition and temperature fields as series of spherical Bessel functions, before solving numerically the linear system of equations obtained from the linearized conservation equations and boundary conditions.

Fig. 1 shows with thick solid lines the growth rate of the translation instability as a function of \mathcal{R}_χ , with $\frac{\alpha_T \Delta\Theta}{\alpha_c \Delta\chi}$ fixed at -3 , $Le = 10^4$ or 2×10^7 , and different forms of the base compositional profile ($r_{ic}^* = 0, 1$, and ∞ in eq. (41)). When \mathcal{R}_χ is increased above the critical value for instability, σ initially increases in proportion to \mathcal{R}_χ before reaching a plateau.

In the limit of $Le \gg 1$, a good approximation of the growth rate σ of the translation instability is given (in dimensional form) by

$$\sigma = \frac{\kappa_T}{r_{ic}^2} \frac{1/3 - 2/5 r_{ic}^*}{2/3 - r_{ic}^*} \frac{\mathcal{R}_\chi / Le}{1 - \frac{\mathcal{R}_\Theta}{175/2}} \quad (50)$$

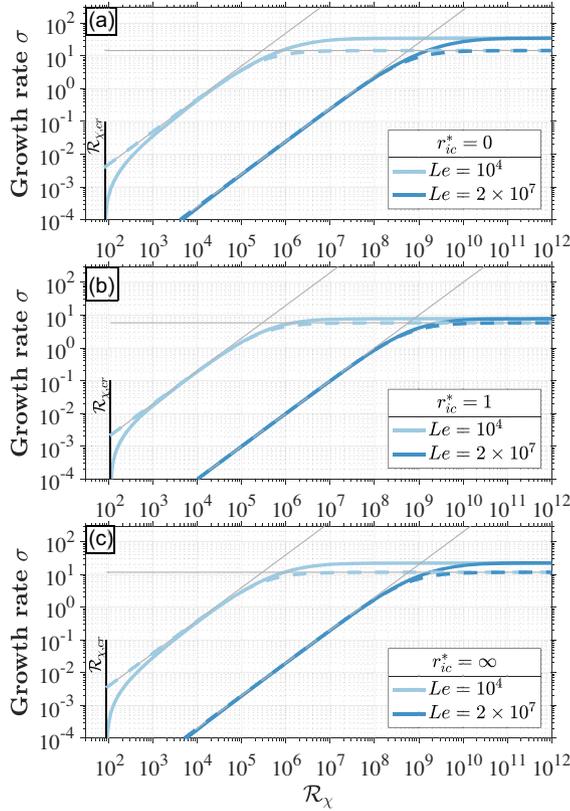


Figure 1. Growth rate of the translation instability as a function of \mathcal{R}_χ at $\frac{\alpha_T \Delta \Theta}{\alpha_c \Delta \chi} = -3$, $Le = 10^4$ or 2×10^7 , and (a) $r_{ic}^* = 0$, (b) $r_{ic}^* = 1$ and (c) $r_{ic}^* = \infty$. The thick solid lines show the numerical solutions of the dispersion equation (A43); the dashed lines show the approximate solution given in eq. (50). The thin grey lines show the two asymptotes given by eq. (51).

(see Appendix A3.3 for the derivation). This has the two following limits:

$$\sigma \simeq \frac{\kappa_T}{r_{ic}^2} \frac{1/3 - 2/5r_{ic}^*}{2/3 - r_{ic}^*} \begin{cases} \mathcal{R}_\chi / Le & \text{if } -\mathcal{R}_\Theta \ll 175/2, \\ \frac{175}{2} \frac{\alpha_c \Delta \chi}{-\alpha_T \Delta \Theta} & \text{if } -\mathcal{R}_\Theta \gg 175/2. \end{cases} \quad (51)$$

The approximate solution eq. (50) is shown on Fig. 1 with thick dashed lines. The thin grey lines show the two asymptotes given by eq. (51). The two asymptotes intersect at $\mathcal{R}_\Theta = -175/2$, the corresponding value of \mathcal{R}_χ being given by $\frac{\alpha_c \Delta \chi}{\alpha_T \Delta \Theta} Le \mathcal{R}_\Theta = -\frac{175}{2} \frac{\alpha_c \Delta \chi}{\alpha_T \Delta \Theta} Le$. The agreement with the full solution (thick solid lines) is excellent for $-\mathcal{R}_\Theta \ll 175/2$. At $-\mathcal{R}_\Theta \gg 175/2$, the approximate solution underestimates the actual growth rate, by up to a factor 3 at $r_{ic}^* = 0$, but is still rather good at r_{ic}^* around 1.

Note that since $\mathcal{R}_\chi / Le \propto 1/\kappa_T$, the growth rate is independent of the thermal and compositional diffusivities if $-\mathcal{R}_\Theta \ll 175/2$. On the other hand, the growth of the instability is limited by the diffusion of the temperature heterogeneity when $-\mathcal{R}_\Theta \gg 175/2$; the growth rate is inversely proportional to the thermal diffusion timescale, but independent of the compositional diffusion timescale.

5 STEADY-STATE TRANSLATION

We now derive expressions for the translation rate in steady-state conditions, still focusing on the limit $\mathcal{P} \rightarrow 0$ described by the set of equation of Section 2.3. The radius of the inner core is assumed to be constant, and so are the heat and composition source terms S_T

and S_c in eqs (1) and (3). In the stability analysis of Section 4, the base potential temperature and composition profiles were imposed, and the definition of the Rayleigh numbers were based on the assumed potential temperature and composition differences across the inner core, which were left unspecified. This cannot be done anymore because the potential temperature and composition profiles now depend on the translation rate, and are therefore outputs of the problem. We, therefore, non-dimensionalize the potential temperature and composition by constructing potential temperature and composition scales $\Delta \Theta$ and $\Delta \chi$ from the heat and composition sources terms:

$$\Delta \Theta = \frac{S_T r_{ic}^2}{6 \kappa_T}, \quad \Delta \chi = \frac{S_c r_{ic}^2}{6 \kappa_c}, \quad (52)$$

which correspond to steady-state conductive profiles.

5.1 Phenomenology

Fig. 2 shows the translation rate V obtained by solving the set of equations corresponding to the rigid inner core limit [eqs (15), (19) and (20)], for various values of \mathcal{R}_χ , Le and of the buoyancy ratio \mathcal{B} defined as the ratio of the production rates of thermal and compositional buoyancy:

$$\mathcal{B} = \frac{\alpha_T S_T}{\alpha_c S_c} = \frac{\mathcal{R}_\Theta}{\mathcal{R}_\chi} Le^2 = \frac{Ra_\Theta}{Ra_\chi} Le^2. \quad (53)$$

(Note that this ratio is different from the ratio $\frac{\alpha_T \Delta \Theta}{\alpha_c \Delta \chi}$ used in Section 4.) Here the compositional field is always assumed to be destabilizing ($\mathcal{R}_\chi > 0$), so $\mathcal{B} > 0$ means that both compositional and thermal fields are destabilizing, while $\mathcal{B} < 0$ means that the compositional field is destabilizing and the thermal field stabilizing. The steady-state potential temperature and composition fields in cross-sections of the inner core are shown in Fig. 3 for three of these calculations (red diamonds denoted a to c on Fig. 2).

Several different regimes are found depending on the relative importances of advection and diffusion of heat and composition, which are measured, respectively, by the thermal Péclet number $Pe_T = Vr_{ic}/\kappa_T$, and compositional Péclet number $Pe_\chi = Vr_{ic}/\kappa_c = Le Pe_T$. The translation rate being normalized by κ_T/r_{ic} , the thermal Péclet number is simply equal to the non-dimensional translation rate, and the compositional Péclet number is equal to the Lewis number times the translation rate. Since we focus on the translation regime, the relevant diffusion timescales are those of a degree 1 heterogeneity. The free-decay thermal diffusion timescale of a degree 1 temperature heterogeneity is $r_{ic}^2/(\alpha_{11}^2 \kappa_T) \simeq r_{ic}^2/(20.2 \kappa_T)$, where $\alpha_{11} \simeq 4.4934$ is the first zero of the degree 1 spherical Bessel function of the first kind.¹ Thermal (resp. compositional) diffusion would, therefore, be small compared to advection if Pe_T (resp. Pe_χ) is large compared to 20.2.

If $\mathcal{B} > -1$, the net buoyancy gradient is destabilizing, and the translation mode is found to be very similar to thermally driven translation: the compositional and thermal fields display degree 1 heterogeneity patterns, which are more or less pronounced depending on the value of the Péclet numbers. Fig. 3(a) shows the composition and potential temperature fields in a case where both

¹The free-decay thermal diffusion timescale is obtained by looking for a solution of the heat equation of the form $\Theta_l(r, t) = \hat{\Theta}_l(r) P_l(\cos \theta) e^{-\lambda t}$. The solution satisfying the condition $\Theta_l(r_{ic}, t) = 0$ is $\hat{\Theta}_l(r, t) = j_l(\alpha_{11} r/r_{ic}) P_l(\cos \theta) e^{-t/(\alpha_{11}^2 \kappa/r_{ic}^2)}$, where j_l is the spherical function of the first kind of degree l and α_{11} its first zero.

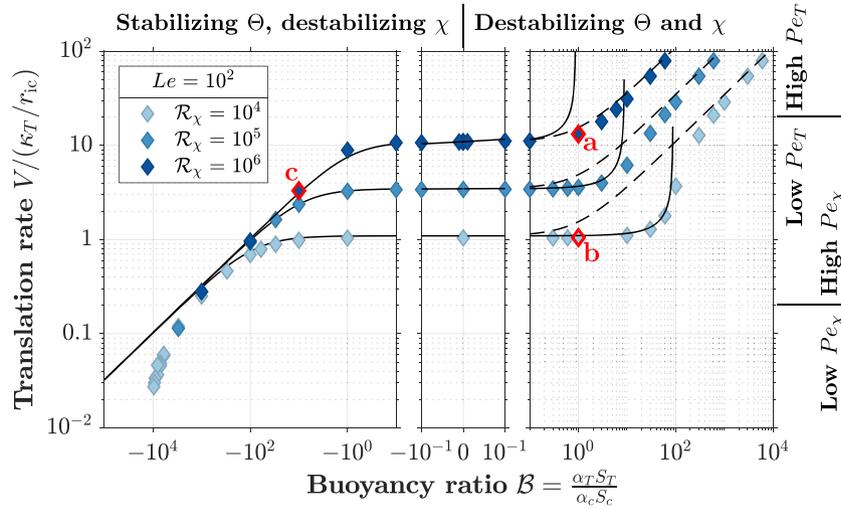


Figure 2. Steady-state translation rate as a function of the buoyancy ratio, Lewis number and compositional Rayleigh number. Filled diamonds show results from the rigid inner core limit numerical model. Black lines are the predictions of the analytical models in the large thermal and compositional Péclet numbers [dashed lines, eq. (57)] and large compositional Péclet number, $\mathcal{O}(1)$ thermal Péclet number [solid lines, eq. (66)] regimes. The red symbols denoted **a** to **c** correspond to the snapshots shown in Fig. 3.

the compositional and thermal Péclet numbers are large compared to 1. The translation rate is $V = 13.2$, which gives $Pe_T = 13.2$ and $Pe_\chi = 1.32 \times 10^3$. The composition and potential temperature fields show a degree 1 pattern with higher concentration and potential temperature on the melting side. The composition and potential temperature go back to zero across a boundary layer on the melting side to satisfy the boundary conditions (the compositional boundary layer cannot be seen on the figure, but is resolved in the numerical calculation). The thermal boundary layer is much thicker, owing to the much larger thermal diffusivity (since the boundary layer is where diffusion balances advection, its thickness is on the order of $1/Pe_T$). Fig. 3(b) shows the composition and potential temperature fields in a case where the compositional Péclet number is large compared to 1 ($Pe_\chi = 105$), while the thermal Péclet number is on the order of 1 ($Pe_T = 1.05$). The compositional field is similar to the case of Fig. 3(a), though the boundary layer is thicker. In contrast, the potential temperature field is only slightly affected by the translation: it is close to a diffusive field, the isotherms being only slightly shifted towards the melting side of the inner core. An expression for the translation rate in this regime is obtained in Section 5.2.

If $B < -1$, we find that the translation mode still exists even though the stabilizing thermal density gradient is now larger in magnitude than the destabilizing compositional density gradient, in agreement with the stability analysis of Section 4. The translation rate—hence the thermal Péclet number—is found to be always smaller than about 10, which means that the Péclet number based on the degree 1 diffusion timescale, $V r_{ic} / (\alpha_{11}^2 \kappa_T)$, is always smaller than ≈ 0.5 . This implies that thermal diffusion is always of importance. This is confirmed by inspection of the potential temperature field pattern. For example, Fig. 3(c) shows the composition and potential temperature fields in a case where $Le = 10^2$, $R_\chi = 10^6$ and $R_\Theta = -10^3$, which gives $B = -10$. The translation rate is $V = 3.3$, which gives $Pe_T = 3.3$ and $Pe_\chi = 330$. The compositional field is very similar to the $B = 1$ cases, but the asymmetry of the potential temperature field is much less pronounced because of the effect of diffusion. This is a distinctive feature of the double-diffusive nature of the translation mode: the translation can perdure only if the degree 1 potential temperature heterogeneity diffuses fast enough for the net buoyancy contribution of the thermal field to

remain smaller than the compositional contribution. In practice, the volume integrated thermal buoyancy almost balances the compositional buoyancy, but thermal diffusion allows a small imbalance which drives the translation. This is similar to the mechanism of the more classical salt finger regime of double-diffusive convection (e.g. Turner 1974), except that it happens at a much larger length scale. In the classical salt finger regime, convection develops in the form of narrow vertical plumes with a width selected by the instability to allow efficient heat diffusion but negligible compositional diffusion (Stern 1960). This has the effect of reducing the stabilizing effect of thermal buoyancy while letting the compositional buoyancy unaffected, hence promoting convection. In the translation regime, the length scale is fixed at $\sim r_{ic}$ (i.e. there is only one 'salt finger'), and the translation rate is limited by the necessity to smooth out the lateral temperature heterogeneities by diffusion. In other words, the translation rate is selected to allow for efficient heat diffusion but negligible compositional diffusion.

We derive in the next two subsections analytical expressions for the translation rate obtained under the assumption that both the thermal and compositional Péclet numbers are large (Section 5.2), or that the compositional Péclet number is large and the thermal Péclet number on the order of 1 or smaller (Section 5.3). The $Pe_\chi \gg 1, Pe_T \gg 1$ case is not relevant for the double-diffusive regime, but would be relevant for the inner core if its thermal history and thermal diffusivity are such that the temperature field is destabilizing. It is also a direct extension of the model of thermal translation developed in Alboussière *et al.* (2010) and Deguen *et al.* (2013), and is therefore useful as a reference. The analytical solutions are shown on Fig. 2 in black dashed lines and black solid lines, respectively. Note that the domain of validity of these solutions are really defined in terms of the Péclet numbers, which depend on the Rayleigh numbers and Lewis number. In particular, the $Pe_\chi \gg 1, Pe_T = \mathcal{O}(1)$ solution is valid in the double-diffusive regime ($B < -1$) but happens to also correctly predict V for the $B > -1$ cases when the translation rate is not too large.

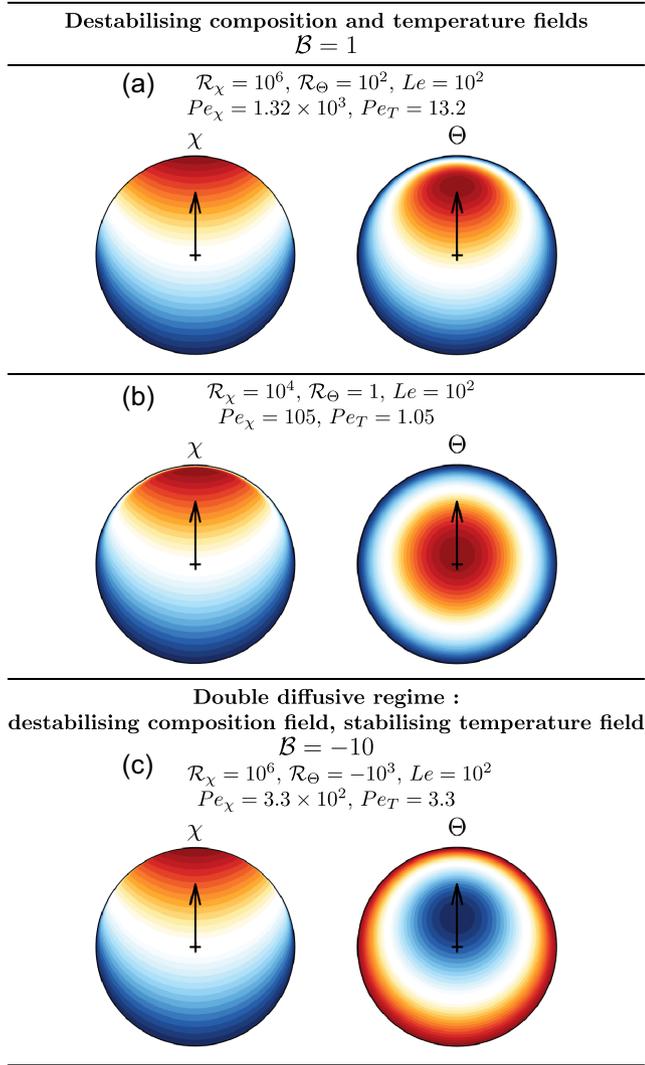


Figure 3. Steady-state composition (left) and potential temperature (right) fields in a cross-section of the inner core including the translation direction, obtained by solving the system of equations corresponding to the rigid inner core limit (Section 2.3). The black arrows show the translation direction. Reds means high potential temperature/composition, and blue means low potential temperature/composition. Panels (a) and (b) show the composition and potential temperature fields in cases where they are both destabilizing. Panel (c) corresponds to a case where the composition field is destabilizing and the potential temperature stabilizing.

5.2 Large thermal and compositional Péclet numbers

We assume here that diffusion of heat and composition are negligible compared to advection (large thermal and compositional Péclet numbers), and look for a steady-state solution of the translation equations. The translation rate is given by eq. (15) as a function of the degree 1 components of the potential temperature and compositional fields, which can be obtained by considering eqs (19) and (20) with $l = 0$, in which diffusion is neglected and a steady state is assumed:

$$0 = -V \frac{1}{3} \left(\frac{2}{r} + \frac{\partial}{\partial r} \right) \Theta_1 + 6, \quad (54)$$

$$0 = -V \frac{1}{3} \left(\frac{2}{r} + \frac{\partial}{\partial r} \right) \chi_1 + 6Le^{-1}. \quad (55)$$

The solutions of these two equations are

$$\Theta_1 = \frac{6}{V} r, \quad \chi_1 = Le^{-1} \frac{6}{V} r. \quad (56)$$

Inserting these expressions into eq. (15) and solving for V gives the following expression for the translation rate:

$$V = \left[\frac{6}{5} \left(\mathcal{R}_\Theta + \frac{\mathcal{R}_\chi}{Le^2} \right) \right]^{1/2} = \left[\frac{6}{5} \frac{\mathcal{R}_\chi}{Le^2} (1 + B) \right]^{1/2}. \quad (57)$$

This is plotted as black dashed lines in Fig. 2. In dimensional form, this writes

$$V = r_{ic} \left(\frac{\rho}{\Delta \rho} \frac{\alpha_T S_T + \alpha_c S_c}{5 \tau_\phi} \right)^{1/2}. \quad (58)$$

The translation rate is independent of the thermal and compositional diffusivities, which is consistent with the assumption of large thermal and compositional Péclet numbers. The $S_c = 0$ limit of eq. (58) corresponds to the translation rate found by Aboussière *et al.* (2010) in the case of a thermally driven translation.

The magnitude of the thermal and compositional degree 1 heterogeneities can be obtained from eqs (56) and (57) and are given (in dimensional form) by

$$\Theta_1 = \frac{S_T r_{ic}}{V} \frac{r}{r_{ic}} = \frac{S_T r_{ic}^2}{\kappa_T} \left[\frac{6}{5} \frac{\mathcal{R}_\chi}{Le^2} (1 + B) \right]^{-1/2} \frac{r}{r_{ic}}, \quad (59)$$

$$\chi_1 = \frac{S_c r_{ic}}{V} \frac{r}{r_{ic}} = \frac{S_c r_{ic}^2}{\kappa_T} \left[\frac{6}{5} \frac{\mathcal{R}_\chi}{Le^2} (1 + B) \right]^{-1/2} \frac{r}{r_{ic}}. \quad (60)$$

5.3 Large compositional Péclet number, $\mathcal{O}(1)$ thermal Péclet number

We now focus on the case of double-diffusive translation, where the potential temperature gradient is stabilizing and larger in magnitude than the destabilizing compositional gradient. In this situation, we can expect the rate of translation to be limited by the diffusion of the degree 1 component of the potential temperature field. While the compositional Péclet number may still be large, the thermal Péclet number is necessarily of order 1 or smaller.

In this limit, we still have

$$\chi_1 = Le^{-1} \frac{6}{V} r, \quad (61)$$

but the degree 1 component of the potential temperature field now results from a balance between production of degree 1 through translation of the degree 0, and diffusion of the degree 1. Θ_1 can be obtained by considering eq. (19) with $l = 1$, which writes

$$0 = -V \frac{2}{5} \left(\frac{3}{r} + \frac{\partial}{\partial r} \right) \Theta_2 - V \frac{\partial \Theta_0}{\partial r} + \mathcal{D}_1 \Theta_1 \quad (62)$$

in steady state. Now since the degree 2 component is produced by the translation of the degree 1 component, which here is assumed to remain small compared to the degree 0 component, the two terms in Θ_2 in eq. (62) are expected to be small compared to the term due to translation of the degree 0. We, therefore, neglect these terms and, recalling that $\Theta_0 = 1 - r^2$, eq. (62) becomes

$$0 = 2Vr + \mathcal{D}_1 \Theta_1, \quad (63)$$

the solution of which [using eq. (44) with $\alpha = 1$ and the boundary condition $\Theta_1 = 0$ at $r = 1$] being

$$\Theta_1 = \frac{V}{5} (r - r^3). \quad (64)$$

Inserting this expression for Θ_1 and the high compositional Péclet number limit for χ_1 into eq. (15) and solving for V gives

$$V = \left(\frac{6}{5} \frac{\mathcal{R}_\chi / Le^2}{1 - \frac{2}{175} \mathcal{R}_\Theta} \right)^{1/2} \quad (65)$$

$$= \left[\frac{5}{6} \left(\frac{Le^2}{\mathcal{R}_\chi} - \frac{2}{175} \mathcal{B} \right) \right]^{-1/2}. \quad (66)$$

This is plotted as black solid lines in Fig. 2. The translation rate approaches $\sqrt{-105/\mathcal{B}}$ if $-\mathcal{R}_\Theta \gg 175/2$. In this limit, the translation rate is, therefore, independent of the phase change timescale. It is instead limited by the rate of diffusion of the degree 1 thermal heterogeneities. Note that in the double-diffusive regime (i.e. $\mathcal{B} < -1$), the translation rate is predicted to be smaller than $\sqrt{105} = 10.25$, which is consistent with the observation from the numerical simulations that V is smaller than $\simeq 10$ in this regime.

In dimensional form, the translation rate writes

$$V = \frac{\kappa_T}{r_{ic}} \left(-\frac{\alpha_c S_c}{\alpha_T S_T} \frac{105}{1 - 525 \frac{\kappa_T^2 \Delta \rho \tau_\phi}{\alpha_T \rho S_T r_{ic}^4}} \right)^{1/2}. \quad (67)$$

The translation rate approaches $(\kappa_T/r_{ic}) \sqrt{-105 \frac{\alpha_c S_c}{\alpha_T S_T}}$ if $-\mathcal{R}_\Theta \gg 175/2$. The magnitude of the degree 1 temperature and composition heterogeneities can be obtained from eqs (61), (64) and (66), and are given by

$$\begin{aligned} \Theta_1 &= \frac{1}{30} \frac{S_T r_{ic}^3}{\kappa_T^2} V \\ &= \frac{1}{30} \frac{S_T r_{ic}^2}{\kappa_T} \left[\frac{105}{-\mathcal{B} \left(1 - \frac{87.5}{\mathcal{R}_\Theta} \right)} \right]^{1/2} \left[\frac{r}{r_{ic}} - \left(\frac{r}{r_{ic}} \right)^3 \right], \end{aligned} \quad (68)$$

$$\chi_1 = \frac{S_c r_{ic}}{V} \frac{r}{r_{ic}} = \frac{S_c r_{ic}^2}{\kappa_T} \left[\frac{105}{-\mathcal{B} \left(1 - \frac{87.5}{\mathcal{R}_\Theta} \right)} \right]^{1/2} \frac{r}{r_{ic}}. \quad (69)$$

5.4 Comparison with numerical calculations

Fig. 2 shows the translation rate obtained from solving numerically eqs (15)–(20) given in Section 2.3 (ignoring any possible deformation of the inner core), together with the predictions of eqs (57) (black dashed lines) and (66) (solid black lines). The agreement is excellent as long as $\mathcal{R}_\Theta/\mathcal{R}_{\Theta,cr} + \mathcal{R}_\chi/\mathcal{R}_{\chi,cr} \gg 1$. The prediction in the $Pe_C \gg 1$, $Pe_T = \mathcal{O}(1)$ limit remains valid when both the thermal and compositional fields are destabilizing as long as the translation rate is smaller than about 10. Above that value, the high Pe_C , high Pe_T prediction is in very good agreement with the numerical solution.

Also shown in Fig. 2 is the value of \mathcal{B} corresponding to the onset of the instability at $Le = 10^2$ according to the marginal stability condition, calculated as follow. The numerical calculations correspond to a case with constant S_χ and S_Θ , for which the critical modified Rayleigh numbers are both equal to 175/2. The marginal stability condition given by eq. (40) then writes

$$\mathcal{R}_\Theta + \mathcal{R}_\chi = \frac{175}{2}, \quad (70)$$

as found in Section 4. In terms of \mathcal{B} , this writes

$$\mathcal{B} = \left(\frac{175/2}{\mathcal{R}_\chi} - 1 \right) Le^2. \quad (71)$$

At $Le = 10^2$ and $\mathcal{R}_\chi = 10^4$, this gives a critical value for \mathcal{B} equal to -9.9×10^3 . This value, shown with a grey line on Fig. 2, is consistent with the onset of the instability obtained numerically.

6 DEFORMATION AND CONDITIONS OF EXISTENCE OF THE TRANSLATION MODE

The advection of heat and composition by the translation mode induces $l = 1$ horizontal density variations (Fig. 3) which may drive a large-scale creeping flow from the melting hemisphere to the crystallizing hemisphere. This would redistribute the temperature and concentration perturbations in a way that weakens the magnitude of the driving force of the convection mode. In the purely thermal case, it was shown (Deguen *et al.* 2013; Mizzon & Monnereau 2013) that the relative importance of this flow and of the translation is a function of \mathcal{P} , with the translation mode collapsing when $\mathcal{P} \gtrsim 30$. In the double-diffusive regime, a similar condition on \mathcal{P} is expected, but the conditions of existence of the translation mode are expected to be more severe because the thermal and compositional buoyancy fields almost balance each other at the global scale, thus leading to a relatively small translation rate, but do not balance at the local scale. This implies that the magnitude of the lateral variations of density—and hence the resulting flow—will be larger, for a given translation rate, than in the purely thermal case.

To quantify the importance of deformation and its effect on the translation mode, we solve numerically the system of equations (introduced in Section 2.2) corresponding to a viscously deforming inner core. Fig. 4 shows a regime diagram constructed from an ensemble of axisymmetric calculations, done at a fixed value of $\mathcal{B} = -3$ and $Le = 10^2$. At fixed \mathcal{B} and Le , the ratio of the thermal and compositional Rayleigh numbers is fixed at $\mathcal{B}Le^{-2}$, so that there are only two independent control parameters, \mathcal{P} and either Ra_χ or Ra_Θ . Though the driver of the convection is the compositional field, the translation mode happens to be limited by the value of Ra_Θ , as demonstrated later in this section [see the discussion surrounding eq. (73)]. We thus show the regime diagram in terms of both Ra_χ (left axis) and $-Ra_\Theta$ (right axis). In Fig. 4, the thick black line corresponds to the onset of the instability obtained from the complete linear stability analysis (Section 4.1), while the thin black line corresponds to the onset of the translation mode only (Section 4.2.1). Fig. 5 shows snapshots of the potential temperature (left) and composition (right) fields from some of the numerical calculations used in building the regime diagram. Also shown in Fig. 5 are streamlines of the velocity field (left) and of the velocity field minus its translation component (right). The streamlines on the left and right sides would look identical if the translation component of the flow is small.

Figs 4 and 5 show that the translation mode is dominant at small values of \mathcal{P} and moderate Rayleigh numbers. The $\mathcal{P} = 0.1$, $Ra_\chi = 10^2$, $Ra_\Theta = -3 \times 10^{-2}$ case in Fig. 5 is one example of this regime. The streamlines of the flow (left panel) are very close to straight lines, which is consistent with a translation, and the potential temperature and composition fields are similar to the numerical solutions obtained in Section 5 in the rigid inner core limit (Fig. 3). The flow is not a pure translation, as can be seen from the right panels showing the streamlines of the non-translation component of

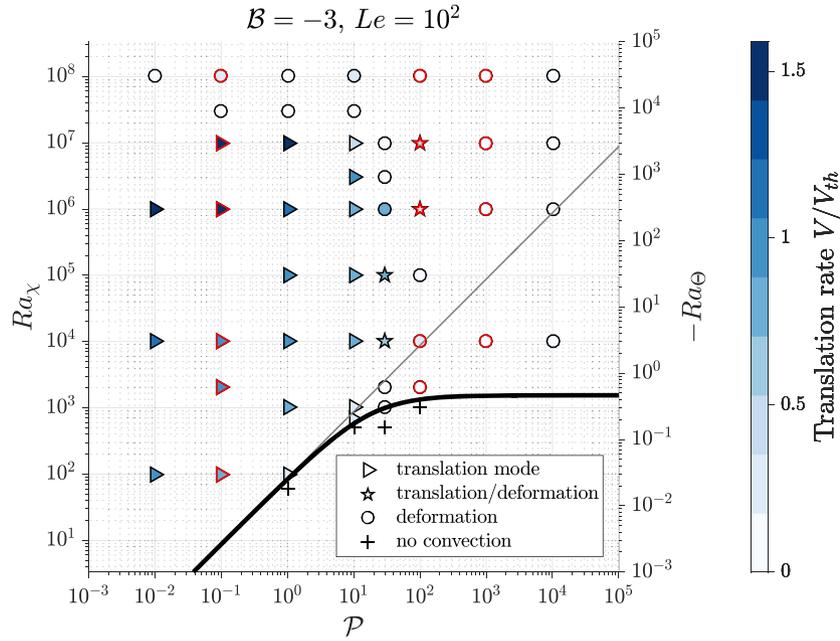


Figure 4. Regime diagram in a (\mathcal{P}, Ra_Θ) space, with $\mathcal{B} = -3$. The colour shading shows the translation rate normalized by the prediction of eq. (66) in the high compositional Péclet, order 1 thermal Péclet regime. \blacktriangleright : calculations in which the translation mode is dominant; \circ : calculations in which the translation component is small compared to the deformation component of the velocity field; \star : calculations in which the translation and deformation components of the velocity field are of similar magnitude; $+$: no convection. The thick black line corresponds to the onset of the instability obtained from the complete linear stability analysis (Section 4.1), while the thin black line corresponds to the onset of the translation mode only (Section 4.2.1). The red symbols correspond to the snapshots shown in Fig. 5.

the flow, which magnitude is small but non-zero (about 1 per cent of the translation rate).

The translation mode appears to be dominant only if $Ra_\chi \lesssim 2 \times 10^7$, $-Ra_\Theta \lesssim 6 \times 10^3$ and $\mathcal{P} \lesssim 30$ (Fig. 4):

(1) Keeping $\mathcal{P} \lesssim 30$, increasing Ra_χ and $-Ra_\Theta$ results in an increase of the degree 1 component of the potential temperature field, and of the relative magnitude of the non-translation component of the flow: at $\mathcal{P} = 0.1$, $Ra_\chi = 10^7$, $Ra_\Theta = -3 \times 10^3$, it is strong enough to deform the streamlines of the flow (left panel), which now significantly deviate from straight lines (the magnitude of the non-translating component of the velocity field is about 20 per cent of the translation rate). Increasing again the Rayleigh numbers, the translation component of the flow disappears almost totally (see the $\mathcal{P} = 0.1$, $Ra_\chi = 10^8$, $Ra_\Theta = -3 \times 10^4$ case in Fig. 5, where no translation component can be seen from the streamlines pattern).

(2) If \mathcal{P} is increased above $\simeq 30$, the convection pattern just above the onset of convection consists in a degree 1 cell (see e.g. the $\mathcal{P} = 10^3$, $Ra_\chi = 10^4$, $Ra_\Theta = -3$ case in Fig. 5). There is no melting or freezing at the ICB, as can be seen from the fact that the streamlines do not cross the ICB. At higher Ra_χ , the convection pattern consists in small-scale plumes originating from the boundary layer below the ICB, and becomes more chaotic (see e.g. the $\mathcal{P} = 10^3$, $Ra_\chi = 10^7$, $Ra_\Theta = -3 \times 10^3$ case in Fig. 5).

The collapse of the translation mode is due to a secondary flow induced by the lateral density variations associated with the potential temperature and composition fields, which redistributes the temperature and composition fields and weakens their degree 1 components, thus decreasing the translation rate. This secondary flow always exists, but its magnitude becomes comparable to the translation rate only if \mathcal{P} or Ra_Θ are large enough.

The critical value of \mathcal{P} is consistent with that obtained in the case of thermal convection (Deguen *et al.* 2013). This transition is due

to the fact that, at fixed Rayleigh numbers, increasing \mathcal{P} decreases the translation rate, and therefore increases the relative importance of the secondary flow.

The fact that the translation also collapses when Ra_χ and $-Ra_\Theta$ are large can be understood as follows: Treating the velocity \mathbf{v} of the secondary flow as a small perturbation of the translation, and using the steady-state composition and potential temperature fields of the double-diffusive regime [eqs (61) and (64)], the Stokes equation (5) can be written as

$$\nabla^2 \mathbf{v} = \nabla p - \left[Ra_\Theta \frac{V}{5} (r - r^3) + \frac{Ra_\chi}{Le^2} \frac{6}{V} r \right] \cos \theta \mathbf{r}. \quad (72)$$

We then divide eq. (72) by the translation rate V and replace V in the buoyancy term by the double-diffusive translation rate given by eq. (65). The term proportional to $Ra_\chi / (Le^2 V^2)$ gives a term $\propto \mathcal{P}$ plus a term $\propto Ra_\Theta$ which combines with the term in Ra_Θ of eq. (72) to give

$$\nabla^2 \frac{\mathbf{v}}{V} - \frac{1}{V} \nabla p = - \left[Ra_\Theta \left(\frac{1}{7} r - \frac{1}{5} r^3 \right) + 5 \mathcal{P} r \right] \cos \theta \mathbf{r}. \quad (73)$$

It is clear from this equation that $|\mathbf{v}|$ would be a significant fraction of V if either $-Ra_\Theta$ or \mathcal{P} is large. We thus expect that the redistribution of the thermal and compositional heterogeneities will have a significant effect on the translation rate if either $-Ra_\Theta$ or \mathcal{P} is large. This is indeed consistent with the results of the numerical calculations. Eq. (73) also suggests that the critical values of \mathcal{P} and Ra_Θ should not depend on the value of \mathcal{B} or Le . From Fig. 4, we find that the critical values of \mathcal{P} and $-Ra_\Theta$ are $\simeq 30$ and $\simeq 6 \times 10^3$, respectively.

If both the compositional and thermal fields are destabilizing, inserting into the Stokes equation the large Pe_C , large Pe_T potential temperature and composition fields [eq. (56)], dividing by V and

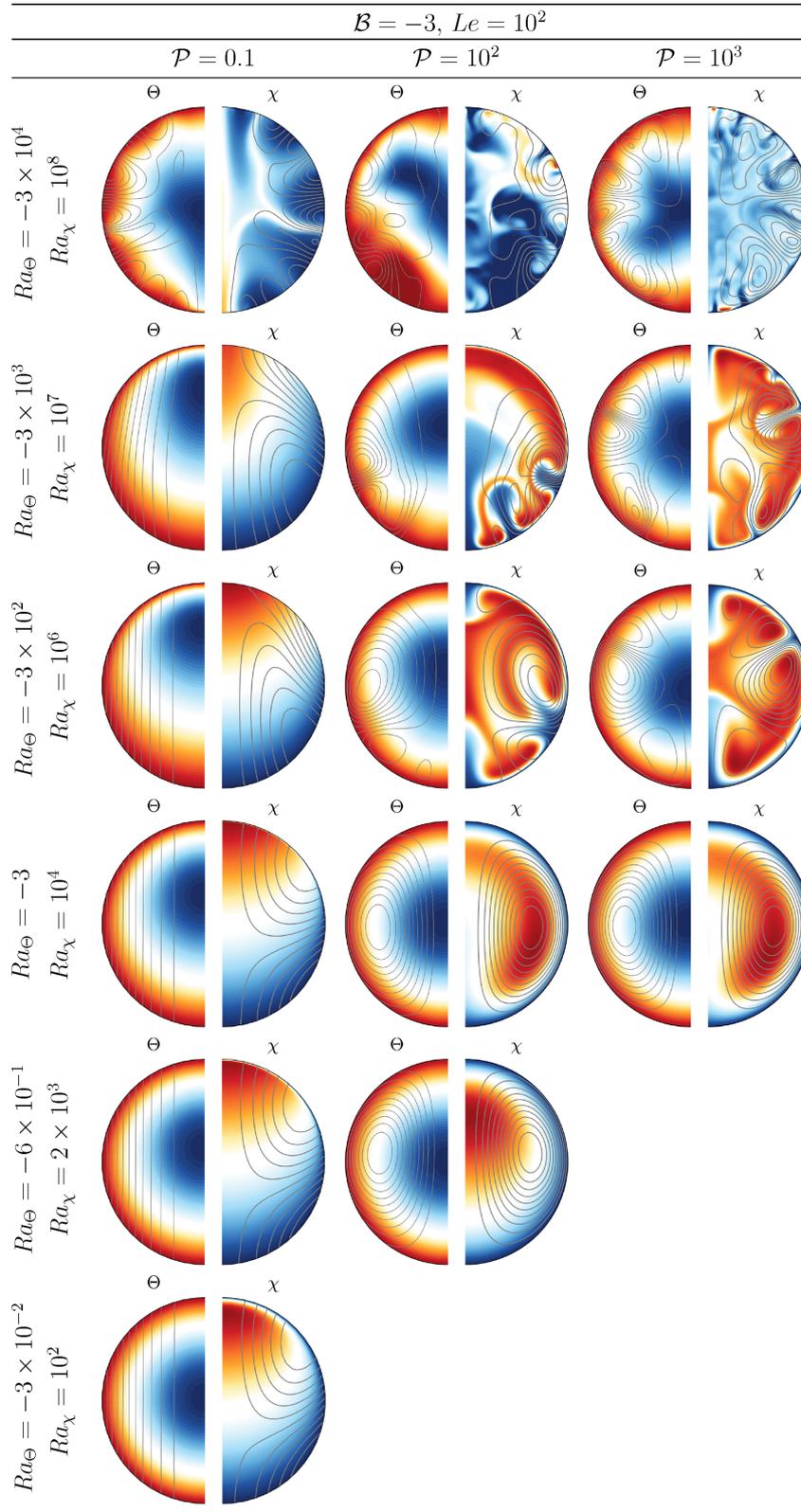


Figure 5. Snapshots of (left) potential temperature (higher values in red, lower values in blue) and streamlines (grey lines) of the flow. Right, light element concentration (higher values in red, lower values in blue) and streamlines (grey lines) of the non-translation component of the flow, for various \mathcal{P} , Ra_Θ , Ra_χ . The snapshots shown here correspond to the numerical solutions denoted by red symbols in the regime diagram shown in Fig. 4. \mathcal{P} increases from left to right, and Ra_χ and $-Ra_\Theta$ increases from bottom to top. \mathcal{B} and Le are kept constant at $\mathcal{B} = -3$ and $Le = 10^2$.

taking the translation rate given by (57) yields

$$\nabla^2 \frac{\mathbf{v}}{V} - \frac{1}{V} \nabla p = -5 \mathcal{P} \cos \theta \mathbf{r} \mathbf{r}, \quad (74)$$

which suggests that in this case, the secondary flow can become a significant fraction of V only if \mathcal{P} is large enough, irrespective of the values of the Rayleigh numbers. This is consistent with the results obtained in the case of a thermally driven translation (Deguen *et al.* 2013).

7 APPLICATION TO EARTH'S INNER CORE

The theoretical and numerical investigations presented in the previous sections show that translation of the inner core in a double-diffusive regime is possible if:

- (1) the compositional and thermal fields are such that

$$\alpha_c \Delta \chi \gtrsim \frac{-\alpha_T \Delta \Theta}{Le} \quad (75)$$

(Section 4). In practice, the value of Le (2×10^7) and $-\alpha_T \Delta \Theta$ are such that even a slightly positive value of $\alpha_c \Delta \chi$ is enough to promote double-diffusive translation. However, the growth rate of the instability and the translation rate do depend significantly on the thermal state of the inner core.

(2) the non-dimensional parameters \mathcal{P} and $-Ra_\Theta$ are smaller than $\simeq 30$ and $\simeq 6 \times 10^3$, respectively (Section 6). These conditions can be rewritten as a condition for the inner core viscosity, which must be larger than

$$\eta_c = \max \left(\frac{\Delta \rho g' r_{ic}^2 \tau_\phi}{30}, -\frac{\alpha_T \rho g' S_T r_{ic}^6}{3.6 \cdot 10^4 \kappa_T^2} \right) \quad (76)$$

for the translation mode to be dominant. The critical viscosity η_c is a strongly increasing function of r_{ic} , which means that this condition is much easier to meet early in the inner core history.

7.1 Thermal evolution of the inner core

The thermal source term S_T can be written as

$$S_T = \frac{\rho g' \gamma T}{2K_S} \left[\left(\frac{dT_s}{dT_{ad}} - 1 \right) \frac{dr_{ic}^2}{dt} - 6\kappa_T \right], \quad (77)$$

where $dT_s/dT_{ad} \simeq 1.65$ is the ratio of the Clapeyron slope to the adiabat, $g' = dg/dr = 3.6 \times 10^{-6} \text{ s}^{-2}$, $\gamma \simeq 1.4$ is the Gruneisen parameter, $K_S = 1400 \text{ GPa}$ the isentropic bulk modulus, $T \simeq 5500 \text{ K}$ the inner core temperature (Deguen & Cardin 2011). For simplicity, instead of solving the core energy balance to obtain the evolution of $r_{ic}(t)$, as was done in Deguen *et al.* (2013), we simply assume an evolution of the form $r_{ic} = r_{ic}^p(t/\tau_{ic})^a$, where $r_{ic}^p = 1221 \text{ km}$ is the present-day radius of the inner core and τ_{ic} is the age of the inner core. Labrosse (2015) found that this expression with a around 0.43 correctly approximates the exact solution of the core energy balance. The advantage of using the simple parametrization is that an explicit form is obtained for S_T , with $dr_{ic}^2/dt = 2a(r_{ic}^p)^2 t^{2a-1}/\tau_{ic}^{2a}$, which makes its evaluation straightforward. For example, with $\kappa_T = 2 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$ (corresponding to a thermal conductivity $\simeq 200 \text{ W m}^{-1} \text{ K}^{-1}$ (Pozzo *et al.* 2014)) and τ_{ic} taken in the range 0.5–1 Gy, we obtain S_T in the range $-1.2 \times 10^{-14} \text{ K s}^{-1}$ to $-8 \times 10^{-15} \text{ K s}^{-1}$. With $\kappa_T = 10^{-5} \text{ m}^2 \text{ s}^{-1}$ (a thermal conductivity $\simeq 100 \text{ W m}^{-1} \text{ K}^{-1}$), this range becomes $-4 \times 10^{-15} \text{ K s}^{-1} < S_T < -9 \times 10^{-16} \text{ K s}^{-1}$. With a diffusivity equal to $\kappa_T = 5 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$ corresponding

to a thermal conductivity $\simeq 50 \text{ W m}^{-1} \text{ K}^{-1}$, S_T is positive (i.e. the temperature field is destabilizing) if $\tau_{ic} < 0.88 \text{ Gy}$.

7.2 Compositional evolution of the inner core

A convenient starting point for discussing the compositional state of the inner core is the logarithmic derivative of the relation $k = c_s/c_l$ expressing thermodynamic equilibrium at the ICB:

$$\frac{dc_s}{c_s} = \frac{dc_l}{c_l} + \frac{dk}{k}. \quad (78)$$

The development of an unstable compositional profile in the inner core requires that $dc_s/c_s < 0$, which depends on both the evolution of the outer core concentration and on the evolution of the partitioning behaviour.

(1) In the standard model of a well-mixed outer core, light elements are preferentially partitioned to the outer core ($k < 1$) and the concentration of these elements builds up in the liquid as the inner core crystallizes. dc_l/c_l is therefore positive. The concentration profile in the inner core can then be destabilizing only if dk/k is negative and larger in magnitude than dc_l/c_l . According to *ab initio* calculations of the partitioning behaviour of oxygen and sulphur (Gubbins *et al.* 2013), the partition coefficients of these elements happen to decrease with decreasing temperature, implying that dk/k is indeed negative. The relative importance of dc_l/c_l and dk/k then depends on the core composition and radius of the inner core (through ICB temperature). Labrosse (2014) showed that the concentration of a given element at crystallization is well approximated by

$$c_s^{\text{icb}} = c_{s,0}^{\text{icb}} (1 + Ar_{ic}^3 - Br_{ic}^2), \quad (79)$$

where A and B are parameters which depend on the element considered and its abundance, and $c_{s,0}^{\text{icb}}$ is the concentration in the inner core at nucleation. The r_{ic}^3 term is associated with the compositional evolution of the outer core, and promotes the formation of a stable compositional profile. The r_{ic}^2 term is due to the temperature dependence of the partition coefficient, and promotes the formation of an unstable compositional profile. Labrosse (2014) found that, for plausible core composition models, oxygen has always a destabilizing contribution while sulfur has a destabilizing contribution only while the inner core radius is smaller than $\simeq 500 \text{ km}$. The net compositional profile becomes stabilizing when the radius of the inner core reaches 600–900 km (depending on the composition of the core). Double-diffusive translation could thus plausibly set in early in the inner core history, but would be unlikely to last until today.

From eq. (79), we find that the composition source term is

$$S_c = -\frac{dc_s^{\text{icb}}}{dt} = -c_{s,0}^{\text{icb}} \left(A \frac{dr_{ic}^3}{dt} - B \frac{dr_{ic}^2}{dt} \right) \quad (80)$$

which we will evaluate for different scenarios in Section 7.4, and use to obtain the translation rate when relevant.

(2) The situation would be more favourable to convection if the light elements concentration of the liquid from which the inner core crystallizes increases at a slower pace than what is predicted under the assumption of perfect mixing of the outer core, or even decreases with time. This may happen for at least three reasons:

(i) If light elements expelled from the inner core do not mix perfectly in the outer core and accumulate in a stably stratified

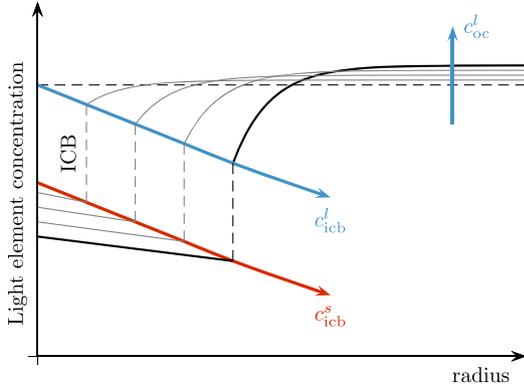


Figure 6. A schematic showing qualitatively the expected effect on the inner core composition of the formation of an iron-rich layer above the ICB. The thin black lines correspond to concentration profiles in the core at different times, with the thick black line corresponding to the current state of the core. The blue and red curves show the evolution of the concentration at the ICB in the solid and liquid phases, respectively. The concentration in the bulk of the outer core increases in response of inner core crystallization, but the concentration at the ICB decreases.

layer below the CMB (e.g. Fearn & Loper 1981; Braginsky 2006; Bouffard *et al.* 2017), the light elements concentration just above the ICB would increase at a slower rate than in the perfect mixing model. The exact evolution of the composition of the bulk of the outer core would depend on the mixing efficiency.

(ii) Core–mantle chemical interactions can buffer the core composition, or even induce a decrease of the concentration of some light elements. In particular, exsolution of MgO or SiO₂ (Badro *et al.* 2016; O’Rourke & Stevenson 2016; Hirose *et al.* 2017; O’Rourke *et al.* 2017) would make the concentration of O and Si progressively decrease as the core cools down.

(iii) Finally, the existence of the F-layer argues for a secular decrease of light elements concentration close to the ICB, if its interpretation as a stably stratified, iron-rich layer formed as a result of inner core growth is correct. Unless the F-layer is of primordial origin (Arkani-Hamed 2017; Jacobson *et al.* 2017), its formation implies that the inner core has been crystallizing from an increasingly iron-rich melt (Fig. 6), irrespectively of its formation mechanism (Gubbins *et al.* 2008; Alboussière *et al.* 2010; Gubbins *et al.* 2011). In this situation, both dc_l/c_l and dk/k are negative and the composition field is always destabilizing.

7.3 Growth rate of the translation instability

Though instability appears almost unavoidable when the compositional profile is destabilizing, whether the translation rate eventually becomes significant depends on the timescale of instability growth (the inverse of the growth rate σ) compared to the duration of the unstable phase, and on the magnitude of the initial perturbations. From eq. (51), the instability growth rate σ is at most 10 to 30 times κ_T/r_{ic}^2 (depending on r_{ic}^*), which corresponds to a timescale of instability growth $1/\sigma$ between ~ 80 and 240 Myr. This is smaller than the age of the inner core, but this does not ensure by itself a significant translation rate. The time needed to reach a given translation rate depends on the magnitude of the initial perturbation, with $1/\sigma$ being the time needed to increase the translation rate by a factor $e \simeq 2.72$. The translation rate increases by a factor of 10 in a time $(\ln 10)/\sigma \simeq 2.3/\sigma$, which is in the range 180–550 Myr. This is of the same order of magnitude than the inner core age, which implies that a relatively strong perturbation is needed to ensure a significant

translation rate is reached. One possible candidate is heterogeneous growth of the inner core (Sumita & Olson 1999; Aubert *et al.* 2008; Aubert 2013; Driscoll 2015). For example, if convection in the outer core imposes a growth pattern with a persisting degree 1 anomaly of amplitude one tenth of the mean solidification rate, it will take about 200 Myr for the translation rate to reach a value similar to the mean inner core growth.

7.4 Possible scenarios

Fig. 7 shows the results of calculations corresponding to two different scenarios for the compositional evolution of the core, as well as two different thermal histories (parametrized by inner core age). The thermal diffusivity is fixed at $\kappa_T = 2 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$ and the radius of the inner core is assumed to grow as $r_{ic} = r_{ic}^p(t/\tau_{ic})^{0.43}$, with $\tau_{ic} = 0.5$ or 1 Gy. The core is assumed to contain 2.42 per cent O and 6.3 per cent S, following Gubbins *et al.* (2013) and Labrosse (2014). The buoyancy source terms $\alpha_c S_c$ and $\alpha_T S_T$ are calculated from eqs (80) and (77) (Figs 7a and d). This is then used to calculate the non-dimensional numbers \mathcal{B} , \mathcal{R}_χ and \mathcal{R}_Θ , from which we obtain the theoretical steady-state translation rate from eqs (57) and (66) (Figs 7b and e). In addition, we compute the translation rate by solving numerically the ‘rigid inner core’ set of equations (Section 2.3), taking into account the growth of the inner core and its thermal and compositional evolution. The instability is initiated numerically by imposing a small initial degree 1 growth heterogeneity V_{in} of either 10^{-12} or $10^{-11} \text{ m s}^{-1}$. Finally, we show in Figs 7(c) and (f) the critical viscosity η_c above which the translation mode is dominant. According to eq. (76), η_c does not depend on the composition field; its evolution is therefore the same in the two scenarios of compositional evolution.

7.4.1 Crystallization from a well-mixed outer core

Fig. 7 (left panel) shows the results of calculations made under the assumption that the outer core is well-mixed.

For the two thermal histories considered here, $\alpha_T S_T$ is negative, except in the very beginning of inner core crystallization. $\alpha_c S_c$ starts positive, but becomes negative when the inner core radius exceeds $\simeq 600$ km. As a result, translation is only possible while $r_{ic} < 600$ km.

The translation rate obtained from the *steady-state* expressions is typically similar to the inner core growth rate. However, this is misleading because the duration of the unstable phase is rather short compared with the timescale of instability growth. Depending on the thermal history considered, it takes between 100 and 200 Myr for the inner core to reach a radius of 600 km. Since the timescale of instability growth is larger than 200 Myr, this implies that the steady state regime is unlikely to be reached. This is confirmed by the results of the numerical solution of the ‘rigid inner core’ set of equations, which shows that in effect the inner core does not reach an appreciable translation rate before becoming stable against the double-diffusive instability. For example, starting with a forced translation with a translation rate of $10^{-11} \text{ m s}^{-1}$ with an inner core nucleating 0.5 Gy ago, the translation rate increases by a factor of merely 1.5 before decreasing quickly. If the inner core started crystallizing 1Gy ago, the translation rate reaches a maximum only 10 per cent higher than the initial perturbation. We therefore conclude that a significant translation is unlikely in this scenario.

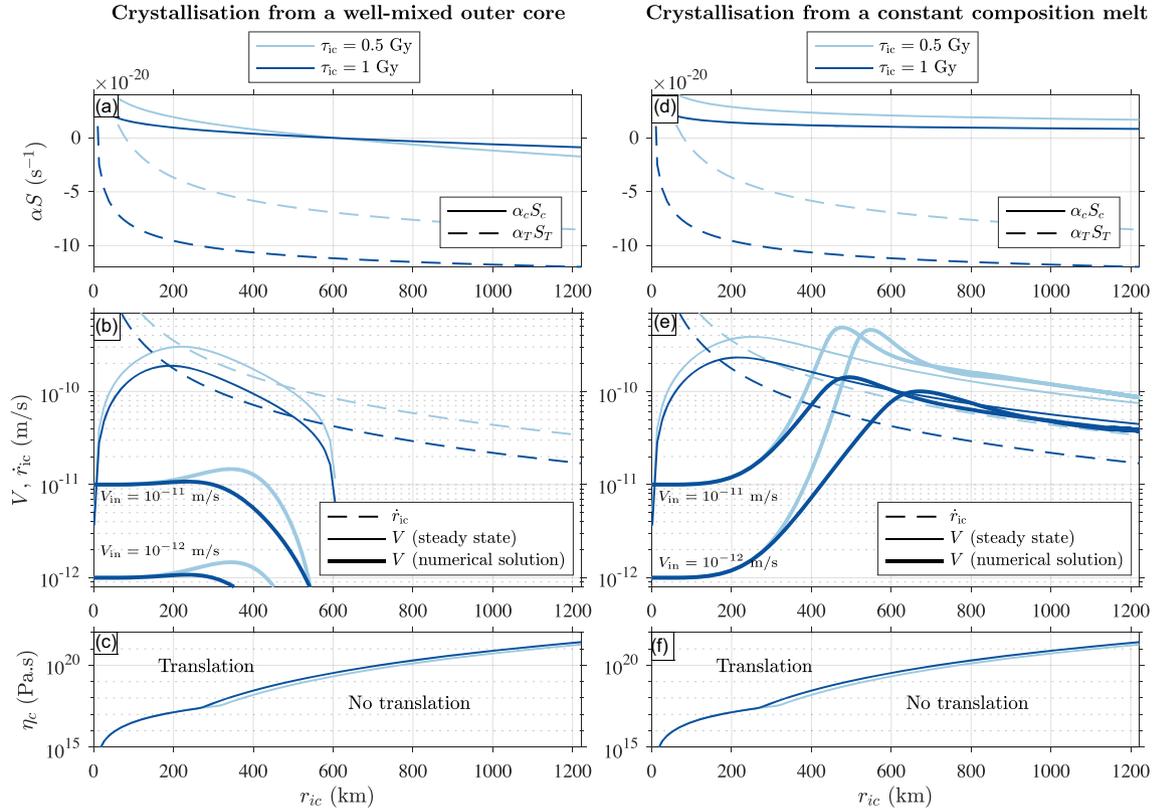


Figure 7. Left column: results of calculations corresponding to a scenario in which the inner core is assumed to crystallize from a well-mixed outer core, the composition of the crystallizing inner core being given by eq. (79). Two thermal histories are considered, with the inner core starting to crystallize either 1 Gy ago (dark blue lines) or 0.5 Gy ago (light blue lines). (a) Solid lines: compositional buoyancy source $\alpha_c S_c$ obtained from eq. (80); dashed lines: thermal buoyancy source $\alpha_T S_T$ obtained from eq. (77). (b) Dashed lines: inner core growth rate \dot{r}_{ic} ; thin solid lines: translation rate obtained from the steady-state solutions [eqs (57) and (66)]; heavy solid lines: translation rate obtained by solving numerically the ‘rigid inner core’ set of equations (Section 2.3), with an imposed degree 1 growth heterogeneity V_{in} of either 10^{-11} m s $^{-1}$ or 10^{-12} m s $^{-1}$. (c) Critical viscosity above which the translation regime dominates [eq. (76)]. Right column: same as panels (a)–(c) if the inner core is assumed to crystallize from a melt of constant composition. The composition of the crystallizing inner core is given by eq. (79) with $A = 0$.

7.4.2 Crystallization from a constant composition melt

Fig. 7 (right panel) shows the results of calculations made under the assumption that the inner core crystallizes from a melt of constant composition, which amounts to taking $A = 0$ in eq. (80).

The thermal histories are the same as in the previous section, $\alpha_T S_T$ being negative for most of the inner core history. However, $\alpha_c S_c$ is now always positive and the inner core is always unstable against the double-diffusive translation instability. The translation rate obtained from the steady-state expressions is typically about two times higher than the inner core growth rate. The translation rate obtained from solving the ‘rigid inner core’ set of equations approaches the steady-state theory after a phase of instability growth, whose duration depends on the magnitude of the initial perturbation. The slight difference between the steady-state theory and the numerical results can be ascribed to the time variation of the inner core radius and source terms.

The critical viscosity η_c above which translation is possible is a strong function of inner core radius. For example, at $r_{ic} = 200$ km, the translation mode is preferred if the inner core viscosity is larger than $\simeq 10^{17}$ Pa s. The critical viscosity strongly increases with radius, and reaches about $2\text{--}3 \times 10^{21}$ Pa s at the current inner-core radius of 1221 km. This does not depend on the composition evolution, and only slightly on the thermal evolution. The final critical viscosity is clearly on the high end part of the range of published estimates, and

marginally within the $10^{20}\text{--}10^{22}$ Pa s range predicted by Reaman *et al.* (2011, 2012). If the viscosity is in the range of 10^{16} to 3×10^{21} Pa s, the inner core may have been in the translation regime during a possibly significant part of its history, before leaving the translation field when the critical viscosity becomes higher than the inner core viscosity.

8 CONCLUSION

We have demonstrated that double-diffusive translation of Earth’s inner core is possible if two conditions are met: (i) the compositional profile within the inner core is destabilizing (almost irrespectively of the thermal state); and (ii) the inner core viscosity is sufficiently large, the required value being a strongly increasing function of the inner core size. The first condition was likely met when the inner core was smaller than about half its present size, and possibly still is if the outer core is imperfectly mixed and has developed stratified regions either below the CMB or above the ICB (Gubbins *et al.* 2013; Labrosse 2014). The second condition is possibly met for a large part of inner core’s history according to the viscosity estimate of Reaman *et al.* (2011, 2012), but would require the inner core viscosity to be larger than 3×10^{21} Pa s to be satisfied today (see Fig. 7).

If these conditions are satisfied, the effective development of the translation instability further requires that: (i) the duration of the

unstable phase is long enough compared to the timescale of instability growth, which can be in the range 200–500 Myr depending on the shape of the compositional profile (see Sections 4.2.2 and 7.3); and (ii) that a perturbation of sufficient magnitude is imposed on the inner core and persists on a timescale similar to the instability growth timescale. The first condition makes the development of double-diffusive translation unlikely in the classical model of compositional evolution of the outer core assuming perfect mixing. However, imperfect mixing of the outer core lengthens the duration of the compositionally unstable phase, potentially enough to allow the development of the translation instability. If the inner core crystallizes from a constant composition melt (Section 7.4.2 and Fig. 7), the compositional profile remains destabilizing up to its current radius. The formation of a stably stratified iron-rich layer above the inner core, as the seismologically observed F-layer could be interpreted, would even increase the destabilizing effect of composition.

In scenarios where the inner core is indeed translating, one interesting feature of the double-diffusive regime is that the translation rate depends predominantly on the thermal diffusivity and buoyancy ratio, and only weakly on the melting/solidification timescale, whose value is more uncertain (Buffett & Matsui 2015). With the thermal and compositional evolution scenarios considered here, the translation rate is found to be typically similar or slightly higher than the inner core growth rate. This is about an order magnitude smaller than what was predicted for a purely thermally driven translation (Alboussière *et al.* 2010; Deguen *et al.* 2013; Mizzon & Monnereau 2013). This happens to be in better agreement with the geodynamo calculations of Aubert *et al.* (2013) and Aubert (2013), which best reproduce the morphology of the Earth's magnetic field with a degree 1 buoyancy flux heterogeneity at the ICB corresponding to a translation rate slightly smaller than the inner core growth rate.

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APPENDIX: GOVERNING EQUATIONS FOR THE TRANSLATION MODE ($\mathcal{P} \rightarrow 0$ LIMIT)

A1 Translation rate

The force balance on the inner core writes

$$0 = \int_V (\rho + \rho') \mathbf{g} dV + \int_S (\boldsymbol{\tau} \cdot \mathbf{n} - P \mathbf{n}) dS, \quad (\text{A1})$$

where ρ is the reference inner core density, ρ' is density perturbations about ρ , and where surface stresses have been decomposed into pressure P and deviatoric stresses $\boldsymbol{\tau} \cdot \mathbf{n}$. Neglecting the small radial variations of ρ , and writing $\mathbf{g} = -\nabla\Psi$, we can transform the volume integral of $\rho\mathbf{g}$ into a surface integral, which gives

$$0 = \int_V \rho' \mathbf{g} dV - \int_S (P + \rho\Psi) dS + \int_S \boldsymbol{\tau} \cdot dS. \quad (\text{A2})$$

Assuming the last integral vanishes (i.e. no net viscous force imposed by the outer core on the inner core and vanishing electromagnetic coupling), the force balance on the inner core comes down to an equilibrium between buoyancy forces associated with density anomalies within the inner core and pressure forces applied by the outer core on the inner core surface. Projecting eq. (A2) on the translation direction, we obtain

$$0 = \frac{\rho g_{\text{icb}}}{r_{\text{ic}}} \int_V (\alpha_T \Theta + \alpha_c \chi) r \cos \theta dV - \int_S (P + \rho\Psi) \cos \theta dS \quad (\text{A3})$$

with the assumption that the gravity acceleration in the inner core is $\mathbf{g} = -g_{\text{icb}}(r/r_{\text{icb}})\mathbf{e}_r$. Here θ is the angle between \mathbf{r} and the translation direction.

Let us denote by $h(\theta)$ the topography of the ICB, defined with respect to a reference isopotential surface that has a mean radius which coincides with the mean inner core radius. In the outer core,

isopressure surfaces coincide with isopotentials, when averaged on timescales long compared to the timescales of outer core dynamics. The pressure applied by the liquid outer core on the ICB is, therefore, given by $P(h) = P_0 - \rho_l g_{\text{icb}} h$, where P_0 is the value of the pressure on the reference isopotential. The gravity potential at the ICB is estimated by expanding $\Psi(h, \theta)$ at first order in h , which gives $\Psi(h, \theta) = \Psi_0 + g_{\text{icb}} h + \mathcal{O}(h^2)$, where Ψ_0 is the value of Ψ on the reference isopotential. Using the above expressions to write P and Ψ at the ICB as functions of h at first order in h , eq. (A3) can be written as

$$\begin{aligned} 0 &= \frac{\rho}{r_{\text{ic}}} \int_V (\alpha_T \Theta + \alpha_c \chi) r \cos \theta dV - \Delta \rho \int_S h \cos \theta dS, \\ &= 2\pi \frac{\rho}{r_{\text{ic}}} \int_0^{r_{\text{ic}}} \int_0^\pi (\alpha_T \Theta + \alpha_c \chi) r^3 \cos \theta \sin \theta d\theta dr \\ &\quad - 2\pi \Delta \rho r_{\text{ic}}^2 \int_0^\pi h \cos \theta \sin \theta d\theta. \end{aligned} \quad (\text{A4})$$

We now expand h , Θ and χ as series of Legendre polynomials of $\cos \theta$ (which correspond to zonal spherical harmonics):

$$h = \sum_{l=0}^{\infty} h_l P_l(\cos \theta), \quad (\text{A5})$$

$$\Theta = \sum_{l=0}^{\infty} \Theta_l(r) P_l(\cos \theta), \quad (\text{A6})$$

$$\chi = \sum_{l=0}^{\infty} \chi_l(r) P_l(\cos \theta). \quad (\text{A7})$$

The Legendre polynomials satisfy the orthogonality condition

$$\int_0^\pi P_l(\cos \theta) P_m(\cos \theta) \sin \theta d\theta = \frac{2\delta_{lm}}{2l+1}, \quad \forall (l, m) \in \mathbb{N}^{+2}, \quad (\text{A8})$$

and since $P_1(\cos \theta) = \cos \theta$, the θ -integrals in eq. (A4) are proportional to the degree 1 coefficient of their integrand. eq. (A4) reduces to an equation giving the degree 1 component of the topography (which is also equal to the displacement of the inner core along the translation direction) as a functions of integrals of the degree 1 temperature and composition heterogeneities:

$$h_1 = \frac{\rho}{\Delta \rho r_{\text{ic}}^3} \int_0^{r_{\text{icb}}} [\alpha_T \Theta_1(r) + \alpha_c \chi_1(r)] r^3 dr. \quad (\text{A9})$$

We can then couple this equation with the phase change law (eq. (10)), giving $V = h_1/\tau_\varphi$, to obtain an expression for the translation rate as a function of the density heterogeneities within the inner core:

$$V = \frac{\rho}{\Delta \rho r_{\text{ic}}^3 \tau_\varphi} \int_0^{r_{\text{icb}}} [\alpha_T \Theta_1(r) + \alpha_c \chi_1(r)] r^3 dr. \quad (\text{A10})$$

A2 Legendre polynomials decomposition of the heat and composition conservation equations

We only allow here for the translation mode, for which the potential temperature and composition fields are symmetric about the translation direction. The equation of transport of heat is then given by eq. (1) in which advective transport is restricted to the translation direction,

$$\frac{\partial \Theta}{\partial t} + V \mathbf{e}_x \cdot \nabla \Theta = \kappa_T \nabla^2 \Theta + S_T, \quad (\text{A11})$$

which can be recast as

$$\frac{\partial \Theta}{\partial t} = -V \cos \theta \frac{\partial \Theta}{\partial r} + V \frac{\sin \theta}{r} \frac{\partial \Theta}{\partial \theta} + \kappa_T \nabla^2 \Theta + S_T. \quad (\text{A12})$$

Defining a new variable $x = \cos \theta$ and substituting in the above equation gives

$$\frac{\partial \Theta}{\partial t} = -Vx \frac{\partial \Theta}{\partial r} + \frac{V}{r} (x^2 - 1) \frac{\partial \Theta}{\partial x} + \kappa_T \nabla^2 \Theta + S_T. \quad (\text{A13})$$

We now decompose Θ as a sum of Legendre polynomials [eq. (A6)], and take the inner product of eq. (A13) with $P_l(x)$, using the orthogonality relation $\int_{-1}^1 P_l^2(x) dx = \frac{2}{2l+1}$ to obtain:

$$\begin{aligned} \frac{2}{2l+1} \frac{\partial \Theta_l}{\partial t} &= -V \int_{-1}^1 x \frac{\partial \Theta}{\partial r} P_l(x) dx \\ &\quad + \frac{V}{r} \int_{-1}^1 (x^2 - 1) \frac{\partial \Theta}{\partial x} P_l(x) dx \\ &\quad + \frac{2}{2l+1} \kappa_T \mathcal{D}_l \Theta_l + \frac{2}{2l+1} S_T \delta_{0l}, \end{aligned} \quad (\text{A14})$$

where the operator \mathcal{D}_l is defined as

$$\mathcal{D}_l = \frac{d^2}{dr^2} + \frac{2}{r} \frac{d}{dr} - \frac{l(l+1)}{r^2}. \quad (\text{A15})$$

Using the recurrence relation

$$x P_n = \frac{n+1}{2n+1} P_{n+1} + \frac{n}{2n+1} P_{n-1} \quad (\text{A16})$$

(Abramovich & Stegun 1965, p. 782), we write the first integral in eq. (A14) as

$$\begin{aligned} \int_{-1}^1 x \frac{\partial \Theta}{\partial r} P_l(x) dx &= \int_{-1}^1 \frac{\partial \Theta}{\partial r} \left(\frac{l+1}{2l+1} P_{l+1} + \frac{l}{2l+1} P_{l-1} \right) dx \\ &= \frac{l+1}{2l+1} \frac{2}{2l+3} \frac{\partial \Theta_{l+1}}{\partial r} \\ &\quad + \frac{l}{2l+1} \frac{2}{2l-1} \frac{\partial \Theta_{l-1}}{\partial r}, \end{aligned} \quad (\text{A17})$$

using again the orthogonality relation.

Using the differential relation

$$(1-x^2) P_n'(x) = -n x P_n + n P_{n-1} \quad (\text{A18})$$

$$= -\frac{n(n+1)}{2n+1} P_{n+1} + \frac{n(n+1)}{2n+1} P_{n-1} \quad (\text{A19})$$

(Abramovich & Stegun 1965, p. 783), we write the second integral as

$$\begin{aligned} \int_{-1}^1 (x^2 - 1) \frac{\partial \Theta}{\partial x} P_l(x) dx &= \sum_{n=0}^{\infty} \Theta_n \int_{-1}^1 (x^2 - 1) \frac{\partial P_n}{\partial x} P_l(x) dx, \\ &= \sum_{n=0}^{\infty} \Theta_n \int_{-1}^1 \left(\frac{n(n+1)}{2n+1} P_{n+1} - \frac{n(n+1)}{2n+1} P_{n-1} \right) P_l(x) dx, \\ &= \frac{2l(l-1)}{(2l-1)(2l+1)} \Theta_{l-1} - \frac{2(l+2)(l+1)}{(2l+1)(2l+3)} \Theta_{l+1}. \end{aligned} \quad (\text{A20})$$

Combining eqs (A17) and (A20), we finally obtain the following expression for the potential temperature transport equation:

$$\begin{aligned} \frac{\partial \Theta_l}{\partial t} = & -V \frac{l+1}{2l+3} \left(\frac{l+2}{r} + \frac{\partial}{\partial r} \right) \Theta_{l+1} \\ & + V \frac{l}{2l-1} \left(\frac{l-1}{r} - \frac{\partial}{\partial r} \right) \Theta_{l-1} \\ & + \kappa_T \mathcal{D}_l \Theta_l + S_T \delta_{0l}, \end{aligned} \quad (\text{A21})$$

A similar equation holds for the evolution of composition.

A3 Growth rate of the translation instability

A3.1 Dispersion equation

We now estimate the growth rate of the instability, by linearizing the heat and composition transport equations, which, similarly as done in Section 4.2.1, we write as

$$\frac{\partial \Theta_1}{\partial t} = -V \frac{\partial \Theta_0}{\partial r} + \mathcal{D}_1 \Theta_1, \quad (\text{A22})$$

$$\frac{\partial \chi_1}{\partial t} = -V \frac{\partial \chi_0}{\partial r} + \frac{1}{Le} \mathcal{D}_1 \chi_1. \quad (\text{A23})$$

The translation rate is given by

$$V = \int_0^1 \left(\mathcal{R}_\Theta \Theta_1 + \frac{\mathcal{R}_\chi}{Le} \chi_1 \right) r^3 dr. \quad (\text{A24})$$

The degree 1 components Θ_1 and χ_1 of the potential temperature and composition fields are expanded as series of spherical Bessel functions of the first kind and order 1, j_1 ,

$$\Theta_1 = \sum_{i=1}^{\infty} A_i^\Theta j_1(\alpha_{1i} r) e^{\sigma t}, \quad (\text{A25})$$

$$\chi_1 = \sum_{i=1}^{\infty} A_i^\chi j_1(\alpha_{1i} r) e^{\sigma t}, \quad (\text{A26})$$

where σ is the growth rate and α_{1i} is the i th zero of j_1 . The functions $r \rightarrow j_1(\alpha_{1i} r)$ for $i = 1, 2, \dots, \infty$ form a complete set of orthogonal functions on $[0, 1]$, and satisfy the orthogonality relation

$$\int_0^1 r^2 j_1(\alpha_{1i} r) j_1(\alpha_{1j} r) dr = \delta_{ij} \frac{\sin^2 \alpha_{1j}}{2\alpha_{1j}^2} \quad (\text{A27})$$

(Chandrasekhar 1961, Chapter 6, section 59). The functions $r \rightarrow j_1(\alpha_{1i} r)$ are eigenfunctions of the operator \mathcal{D}_1 [eq. (21)], such that

$$\mathcal{D}_1 j_1(\alpha_{1i} r) = -\alpha_{1i}^2 j_1(\alpha_{1i} r). \quad (\text{A28})$$

Inserting eqs (A25) and (A26) into eq. (A24) gives

$$V = \sum_{i=1}^{\infty} \left(\mathcal{R}_\Theta A_i^\Theta + \frac{\mathcal{R}_\chi}{Le} A_i^\chi \right) e^{\sigma t} \int_0^1 j_1(\alpha_{1i} r) r^3 dr, \quad (\text{A29})$$

$$= - \sum_{i=1}^{\infty} \frac{\sin \alpha_{1i}}{\alpha_{1i}^2} \left(\mathcal{R}_\Theta A_i^\Theta + \frac{\mathcal{R}_\chi}{Le} A_i^\chi \right) e^{\sigma t}, \quad (\text{A30})$$

where eq. (A33) of Deguen *et al.* (2013) has been used to calculate the integral on RHS of eq. (A29).

The coefficients A_i^Θ and A_i^χ are obtained by inserting eqs (A25) and (A26) into eqs (A22) and (A23)

$$\sum_i A_i^\Theta (\sigma + \alpha_{1i}^2) j_1(\alpha_{1i} r) = -V \frac{\partial \Theta_0}{\partial r}, \quad (\text{A31})$$

$$\sum_i A_i^\chi \left(\sigma + \frac{\alpha_{1i}^2}{Le} \right) j_1(\alpha_{1i} r) = -V \frac{\partial \chi_0}{\partial r}. \quad (\text{A32})$$

before multiplying with $j_1(\alpha_{1i} r)$ and applying the orthogonality relation eq. (A27) to obtain

$$A_i^\Theta = - \frac{2\alpha_{1i}^2 V}{(\sigma + \alpha_{1i}^2) \sin^2 \alpha_{1i}} \int_0^1 \frac{\partial \Theta_0}{\partial r} j_1(\alpha_{1i} r) r^2 dr, \quad (\text{A33})$$

$$A_i^\chi = - \frac{2\alpha_{1i}^2 V}{(\sigma + \alpha_{1i}^2/Le) \sin^2 \alpha_{1i}} \int_0^1 \frac{\partial \chi_0}{\partial r} j_1(\alpha_{1i} r) r^2 dr, \quad (\text{A34})$$

Inserting the above expressions for A_i^Θ and A_i^χ into eq. (A30) gives the following equation for σ :

$$\begin{aligned} \mathcal{R}_\Theta \sum_{i=1}^{\infty} \frac{2}{(\sigma + \alpha_{1i}^2) \sin \alpha_{1i}} \int_0^1 \frac{\partial \Theta_0}{\partial r} j_1(\alpha_{1i} r) r^2 dr \\ + \mathcal{R}_\chi \sum_{i=1}^{\infty} \frac{2}{(Le\sigma + \alpha_{1i}^2) \sin \alpha_{1i}} \int_0^1 \frac{\partial \chi_0}{\partial r} j_1(\alpha_{1i} r) r^2 dr = 1. \end{aligned} \quad (\text{A35})$$

With the base state profiles

$$\Theta_0 = 1 - r^2, \quad (\text{A36})$$

$$\chi_0 = \frac{\frac{3}{2} r_{ic}^* (1 - r^2) - (1 - r^3)}{\frac{3}{2} r_{ic}^* - 1}, \quad (\text{A37})$$

we obtain

$$\int_0^1 \frac{\partial \Theta_0}{\partial r} j_1(\alpha_{1i} r) r^2 dr = 2 \frac{\sin \alpha_{1i}}{\alpha_{1i}^2} \quad (\text{A38})$$

$$\int_0^1 \frac{\partial \chi_0}{\partial r} j_1(\alpha_{1i} r) r^2 dr = 2 \frac{\sin \alpha_{1i}}{\alpha_{1i}^2} \mathcal{F}(r_{ic}^*, \alpha_{1i}) \quad (\text{A39})$$

where

$$\mathcal{F}(r_{ic}^*, \alpha_{1i}) = \frac{1 - \frac{4}{\alpha_{1i}^2} \left(1 + \frac{2}{\alpha_{1i}^2} - \frac{2}{\alpha_{1i} \sin \alpha_{1i}} \right) - r_{ic}^*}{2/3 - r_{ic}^*}. \quad (\text{A40})$$

When deriving eqs (A38) and (A39), we have made use of the relations

$$\int_0^1 j_1(\alpha_{1i} r) r^3 dr = - \frac{\sin \alpha_{1i}}{\alpha_{1i}^2}, \quad (\text{A41})$$

$$\int_0^1 j_1(\alpha_{1i} r) r^4 dr = - \frac{(\alpha_{1i}^4 - 4\alpha_{1i}^2 - 8) \sin \alpha_{1i} + 8\alpha_{1i}}{\alpha_{1i}^6}, \quad (\text{A42})$$

[eq. (A41) is demonstrated in Deguen *et al.* (2013); eq. (A42) can be verified by direct integration].

Finally, inserting eqs (A38) and (A39) into eq. (A35) gives the following dispersion equation

$$\mathcal{R}_\Theta \sum_{i=1}^{\infty} \frac{4}{\alpha_{1i}^2 (\sigma + \alpha_{1i}^2)} + \mathcal{R}_\chi \sum_{i=1}^{\infty} \frac{4 \mathcal{F}(r_{ic}^*, \alpha_{1i})}{\alpha_{1i}^2 (Le\sigma + \alpha_{1i}^2)} = 1. \quad (\text{A43})$$

A3.2 Marginal stability

The critical values of \mathcal{R}_Θ and \mathcal{R}_χ can be obtained by setting $\sigma = 0$ into eq. (A43), which then writes

$$\frac{\mathcal{R}_\Theta}{\mathcal{R}_{\Theta,cr}} + \frac{\mathcal{R}_\chi}{\mathcal{R}_{\chi,cr}} = 1, \quad (\text{A44})$$

where

$$\mathcal{R}_{\Theta,cr} = \frac{1}{4} \left[\sum_{i=1}^{\infty} \frac{1}{\alpha_{1i}^4} \right]^{-1}, \quad (\text{A45})$$

$$\mathcal{R}_{\chi,cr} = \frac{1}{4} \left[\sum_{i=1}^{\infty} \frac{\mathcal{F}(r_{ic}^*, \alpha_{1i})}{\alpha_{1i}^4} \right]^{-1}, \quad (\text{A46})$$

which can be used to verify the consistency of the dispersion eq. (A43) with the results obtained in Section 4.2.1 for the marginal state. Using the results of Sneddon (1960) that $\sum_{i=1}^{\infty} \alpha_{1i}^{-4} = 1/350$, we obtain

$$\mathcal{R}_{\Theta,cr} = \frac{1}{4} \left(\sum_{i=1}^{\infty} \frac{1}{\alpha_{1i}^4} \right)^{-1} = \frac{175}{2} \quad (\text{A47})$$

as was found in Section 4.2.1. It can be verified by computing the sum in eq. (A46) that is consistent with the expression

$$\mathcal{R}_{\chi,cr} = 80 \frac{\frac{3}{2}r_{ic}^* - 1}{\frac{48}{35}r_{ic}^* - 1} \quad (\text{A48})$$

found in Section 4.2.1.

A3.3 Growth rate

To estimate the growth rate of the translation instability, the dispersion eq. (A43) can be solved numerically (with truncated sums) for given values of \mathcal{R}_Θ and \mathcal{R}_χ . The results are shown as thick continuous lines of Fig. 1. An analytical approximation of the growth rate can be obtained as follows.

In the limit of $Le \gg 1$, diffusion of the compositional field can be neglected. In this limit the composition equation (A23) then reduces to

$$\frac{\partial \chi_1}{\partial t} = -V \frac{\partial \chi_0}{\partial r}, \quad (\text{A49})$$

from which we obtain

$$\chi_1 = -\frac{V}{\sigma} \frac{\partial \chi_0}{\partial r} \quad (\text{A50})$$

by noting that by construction $V \propto e^{\sigma t}$.

We further assume that the temperature field is in a quasi-steady state in which the production of degree 1 through translation of the degree 0 is almost exactly balanced by diffusion of the degree 1. This amounts to assumption that the timescale of instability growth $1/\sigma$ is large compared to the timescale of diffusion of a degree one heterogeneity. Under this assumption, eq. (A23) reduces to

$$0 = -V \frac{\partial \Theta_0}{\partial r} + \mathcal{D}_1 \Theta_1. \quad (\text{A51})$$

With $\Theta_0 = 1 - r^2$, the solution is

$$\Theta_1 = \frac{V}{5}(r - r^3). \quad (\text{A52})$$

Inserting eqs (A50) and (A52) into eq. (A24) and evaluating the integrals gives

$$V = \frac{\mathcal{R}_\Theta}{175/2} V + \frac{1/3 - 2/5r_{ic}^*}{2/3 - r_{ic}^*} \frac{\mathcal{R}_\chi V}{Le \sigma}, \quad (\text{A53})$$

from which we obtain

$$\sigma = \frac{1/3 - 2/5r_{ic}^*}{2/3 - r_{ic}^*} \frac{\mathcal{R}_\chi / Le}{1 - \frac{\mathcal{R}_\Theta}{175/2}}. \quad (\text{A54})$$

Fig. 1 shows both the numerical solution of (A43) and the approximate solution given by eq. (A54). The agreement is excellent at small values of σ , and fair though not perfect at large values of σ , a consequence of the thermal quasi-steady state assumption becoming less justified.